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IRAS

CHOPPED PHOTOMETRIC CHANNEL IMAGE

83-004A-03A



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This data set Catalog consists of one magnetic tape. The tape is 9-track, 1600 BPI, ASCII, written in FITS format. The tape contains 3020 files of data.

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Laboratory for  
**SPACE RESEARCH GRONINGEN**  
of the  
National Institute for Space Research

**IRAS-DAX**  
**Chopped Photometric Channel,**  
**Explanatory Supplement**

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## TABLE OF CONTENTS

- 1. Introduction
  - 1.1 Functional description of CPC and IRAS
  - 1.2 Instrument performance
  - 1.3 Product
  - 1.4 Document structure
- 2. Observations
  - 2.1 Observation modes
  - 2.2 Control accuracy
- 3. End products
- 4. The photometer
- 5. Instrument performance
  - 5.1 Detector behaviour
  - 5.2 Sensitivity
  - 5.3 Observed beam profile
- 6. Data reduction
  - 6.1 Input data base
  - 6.2 System design
  - 6.3 Demodulation and deglitching
  - 6.4 Responsivity variation
  - 6.5 Pointing reconstruction and regridding
  - 6.6 Calibration and generation of end products
- 7. Analysis of reduction techniques
  - 7.1 Demodulation and deglitching
  - 7.2 Responsivity variation
  - 7.3 Attitude reconstruction and regridding
  - 7.4 Theoretical beam profile
- 8. Photometric calibration
  - 8.1 Sensitivity changes and repeatability
  - 8.2 Linearity and absolute calibration
  - 8.3 NGC 6543 as reference source
- Annex 1. Deglitching algorithm
- Annex 2. Discussion of sample maps
- Annex 3. Tape format
- Annex 4. List of observations

## 1. Introduction

This document is intended to provide the user of IRAS-CPC observations with the technical information that might be needed in the interpretation of CPC maps.

### 1.1. Functional description of CPC and IRAS

The main goal of the IRAS mission was to make a complete survey of the infrared sky. The "survey instrument" was used for this. (see the Explanatory Supplement to the IRAS Catalogs and Atlases, 1985 (abbreviated as IRASES)). In addition it was possible to perform pointed observations both with the survey instrument and with CPC.

CPC literally means Chopped Photometric Channel. The instrument measures simultaneously in two wavelength bands, one centred at 50  $\mu\text{m}$ , the other at 100  $\mu\text{m}$ . These bands are shown in Fig 4.1. It has a circular field of view with a diameter of 1.2 arcmin, matched to the diffraction limit of the telescope at 100  $\mu\text{m}$ . The CPC, contrary to the survey instrument, was chopping against a reference blade at a few Kelvins.

The CPC mainly distinguishes itself from the survey instrument by its high spatial resolution. The CPC beam is theoretically predicted in chapter 7.4 and observationally derived in chapter 5.3. The observed beam appears to be significantly larger than expected. This can possibly be ascribed to the responsivity variation phenomenon described below.

Generally maps covered a region of 12  $\times$  9 arcmin. These maps were made by executing "raster scans" (see section 2.1) using the satellite attitude control system. Reconstruction of the map (see section 6.5) gives an accuracy of a few arcsec for relative positions within one map, and an absolute accuracy of about 30 arcsec.

### 1.2. Instrument performance

A brief overview of the major items is presented. A more extensive discussion is given in chapter 5. Two major instrumental problems were encountered: responsivity variations and glitches. A common origin for these problems is most likely the too low temperature of the focal plane. In order to understand how these problems affect the astronomical interpretation of the CPC maps a few maps are extensively discussed in Annex 2.

In the course of an observation (4 to 7 minutes) the CPC sensitivity changes when significant infrared flux was "seen" by the detector: we interpret this as a responsivity variation of the detector/FET combination. There are at least two time scales involved: an overall gradual increase of the response if sufficiently strong background radiation is present, and a faster response change due to point sources.

An extra complicating factor to the detector responsivity variations is a DC leak in one of the two extra beams present for beam switching (never used in orbit). Regions exhibiting a complicated structure in the infrared can appear quite weird because of the direct gain changes combined with the DC-leak-caused gain changes.

Two kinds of "glitches" severely affect the raw data: induced by high energy particles, and caused by the infrared photons themselves. Their signature is usually much narrower than expected from a point source.

The reproducibility of observations is generally good.

### 1.3. Product

One of the main requirements on the data processing was that by end '84 a reduced product was available. This inevitably led to compromises in the optimal choice of reduction algorithms and procedures (in spite of the production delay of several months). We are confident about the deglitching, regridding, attitude reconstruction, and calibration, but the correction for the responsivity variations is unsatisfactory at present. Maps that clearly suffer from this effect, after our (too) simple gain-correction procedure, are omitted from the set of maps offered to the IRAS community. We advise people interested in specific suppressed maps (a complete list of observations is added as Annex 4) to contact the Laboratory for Space Research. Special processing tools are available to analyze such maps.

### 1.4. Document structure

The document is split in two parts. The first three chapters are essential reading for any CPC user: the major instrumental problems are briefly described, the observational method is outlined, and the data products are presented.

The subsequent chapters 4 to 8, and the Annexes give background information for the interested reader:

- the instrument and its performance in chapters 4 and 5,
- the data reduction and the analyses leading to reduction methods and algorithms in chapters 6 and 7,
- the flux calibration and linearity in chapter 8,
- several special topics in the Annexes.

## 2. Observations

This chapter describes the observation modes used, and addresses the control accuracy. Characteristics of the CPC instrument are summarized in chapter 1, and elaborately described in chapters 4 and 5.

### 2.1. Observation modes

The IRAS satellite performed observations by scanning at constant solar aspect angle. Special observations employed a "raster scan". A raster scan consisted of a number of small scans ("legs"). Size and shape of the area of sky covered by the legs (a "map") could be chosen almost at will. Many options were not sensible for CPC. All CPC raster scans (summarized in Table 2.1) covered a "rectangular" sky area and reversed the scan direction between legs.

Table 2.1. CPC science raster scans

Name	area in × cr (arcmin)	samples in × cr	separation in cr (arcsec)	occurrence
CPP00A	3 × 1	78 × 10	2.3	6.0
CPPFOA	3 × 1	38 × 10	4.7	6.0
CPC03A	3 × 3	78 × 10	2.3	18.0
CPCF3A	3 × 3	38 × 10	4.7	18.0
CPC09A	9 × 9	38 × 18	14.2	30.0
CPCF9A	9 × 9	18 × 18	30.0	30.0

in: in scan; cr: cross scan,

There are two samples in every second for all types of raster scan.

10 extra samples are taken between raster legs during the turnaround. Inclusion of these samples leads to an in-scan extension of the maps of a few arc minutes.

The astronomer/planner had to code his intended raster scan in the Observation Input Language (OIL). Via a number of computer programs running on a computer at the Ground Operations Centre in Chilton, England the raster scan description in OIL was translated into the data words uplinked to the onboard computer program, as part of the Satellite Operations Plan (SOP). (Such a SOP was executed in about twelve hours, between successive passes of the IRAS satellite in its sunsynchronous orbit.)

There were several reasons to define - for science observations - only a limited number of standard raster scans. Allowing astronomers/planners to choose from a very large number of raster scans for thousands of special observations would have made the task of installing the observations in the ground system almost unmanageable. It proved to be very worthwhile to have many observations executed in exactly the same way: the calibration can depend on the specific raster scan used.

In detail, the CPC observations were done as follows. A position calibration star was observed with the visual sensors in the focal plane, then the satellite slewed to the desired region and performed the raster scan, subsequently the detector looked for a minute at the internal (flux) calibration source, finally the satellite slewed again towards a position calibration star and observed it. The position calibrations can occasionally give an erroneous result (wrong star, wrong catalog position of star) or one or both are absent because of planning constraints. Such problems can result in bad reconstructed positions.

## 2.2. Control accuracy

Astronomers indicated to the planning system the central coordinates (in Ra, Dec) of the region they wanted to study; we refer to "target" position. Of interest to the CPC user is how the coordinates assigned to the processed CPC map are related to this target position.

We defined a fixed grid of pixels on the sky. Attitude reconstruction and regridding (see section 6.5) resulted in surface brightness values being assigned to pixels covered by the raster scan. Within a map the positions are accurate to about 20" with respect to each other.

The accuracy of the location of a map on the sky was derived as follows. We compared for 50 clearcut point sources the position of the source in the CPC map with the target position (assuming that the -usually - optical position coincides with the far-infrared position). This gave a standard deviation of 25" both in-scan and cross-scan. However, the distribution of the position difference values does not resemble a gaussian; it has a more pronounced tail. There are 7 of the 50 observations that have a difference of 60" or slightly more between the target position and the CPC position.

### 3. End products.

About 2100 scientific observations were done during the IRAS mission. After the reduction about 1500 observations were considered acceptable for publication. All observations done with raster scan types other than CPC09A and CPCF9A were left out. Other observations were recognized as problematic during the reduction (usually because of peculiar responsivity variations), and rejected for that reason. Detailed information about the reduction is given in chapter 6.

One reduced observation is presented as 4 maps of the sky. Two of the maps are the result of the full data reduction scheme, for the 50 and 100  $\mu\text{m}$  channels (the 'clean image'). The other two give the corresponding 'raw image' of the same observational data, but here the deglitching and responsivity variation correction steps of the reduction are skipped. Because of the many assumptions involved in these two reduction steps (see chapter 7), we advise the user of the CPC products to compare the two images in order to get an idea of the nature of these corrections. This may help to identify some of the reduction problems outlined in chapter 7. The discussion in Annex 2 of some sample maps clearly shows the need for the combined use of both 'raw' and 'clean' images.

The images are distributed on magnetic tape in the format known as FITS (Flexible Image Transport System, Wells 1981). The total data volume consists of three tapes, containing 489, 624, and 395 observations (the sky has been divided in three equal right ascension parts). The four maps of each observation are organized as two consecutive files on tape. The 50 and 100  $\mu\text{m}$  'clean image' maps are combined into the first file as two planes of typically 40x40 pixels on a common 20 arcsec grid. The 'raw image' maps follow in the second file in exactly the same structure as the clean maps. An example of the FITS header is given in Annex 3.

#### 4. The photometer

The photometer has a field of view matched to the diffraction image of the IRAS telescope in the 100- $\mu\text{m}$  range. The image of the field stop in the telescope focal plane is circular, with a diameter corresponding to 1.2 arc-min. The resulting beam profiles are discussed in section 7.4 and observations pertaining to the beam are described in section 5.3.

The optics and the detectors with their pre-amplifiers are in an assembly cooled to 2.4 K.

An absolute chopper, operating at about 15 Hz, is located just in front of the field stop. Thus the infrared signal modulation is proportional to the difference in emission from the sky and from the cold chopper blades. The chopper is of the tuning-fork type, with a shutter blade fixed to each of its tines.

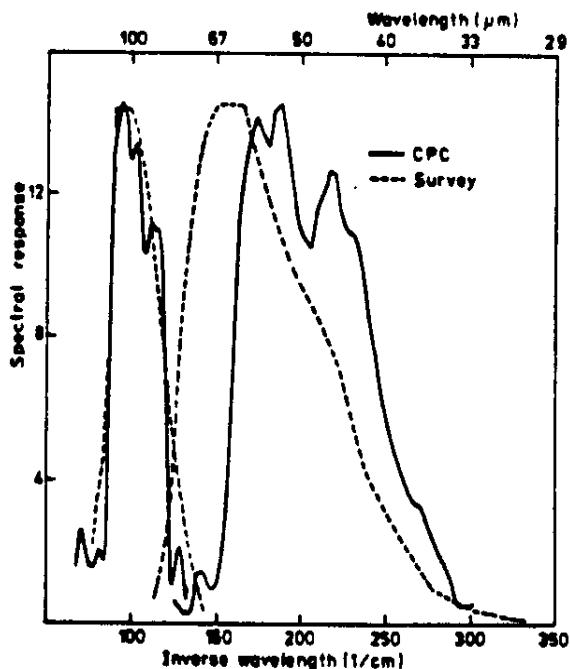


Fig. 4.1. The spectral response of CPC and of the survey instrument.

An optical system consisting of a beam splitter, filters and field optics images the telescope pupil onto the two detectors. The combination of beam splitter, filters and detector cut-offs define the wavelength bands (41-62.5 and 84-114 microns). The resulting passbands are shown in Fig. 4.1. Short-wavelength leaks, if present, are at most at the one percent level, as is evident from observations of Ceres and of stars.

Both detectors were made from Gallium-doped Germanium; they were operated at a bias voltage of 40 mV.

The pre-amplifiers are of the trans-impedance type. They are followed by a spike-suppression circuit (operating in the millisecond domain) and by a

15-Hz bandpass filter. The 15-Hz signals then pass though a zero-clamping circuit, which essentially rectifies without integrating, are converted to a logarithmic scale and finally digitized and sampled at 64 Hz. The digitization steps correspond to increments of 3.5 %.

A third 64-Hz data channel records a reference signal from the chopper drive electronics.

A more detailed description of the instrument is given by Wildeman, Beintema and Wesselius (1983).

The instrument provides options that were not used during the mission, intended to solve potential dynamic-range problems. One of these, a differential chopping mode, is relevant because of a non-modulated optical path via an additional aperture, compounding the problem of responsivity variations. The offending aperture is located at a distance of 2.25 arcminutes; on average, it contributes 40 % of the background radiation.

## 5. Instrument performance

In the first section there is an extensive discussion on responsivity variation and the effect of glitches. These two detector problems were not expected and seriously affect the quality of the CPC data. The sensitivity of the CPC is described in section 5.2, while section 5.3 addresses the beam profile.

Calibration of the CPC, sensitivity changes, and repeatability are treated in chapter 8.

### 5.1. Detector behaviour

#### 5.1.1. Introduction

Both CPC detectors behaved anomalously during the flight: their sensitivity was much too low, they exhibited strong signal-dependent spiking and their responsivity was strongly influenced by the incoming flux. These effects must be related to the unexpectedly low instrument temperature (2.4 K instead of 3.5 K): one single observation at the end of the mission, when the cryogen was exhausted and the instrument started to warm up, was of a much higher quality. However, the effects are not understood physically and could not be reproduced under laboratory conditions.

#### 5.1.2. Spiking

The spiking phenomenon is the likely cause of the loss of sensitivity and it is probably connected with the responsivity variations. Most of the spiking was clearly correlated with the amount of incident infrared flux. Moreover, spikes tended to occur during the "open" phase of the chopper cycle: even if phase-sensitive demodulation was applied, spiking would always increase the over-all instrument response. In effect spiking represented an erratic component in the detector responsivity; in an observation on a strong point source, obvious spikes, if left in the data, could contribute 10 % of the observed flux.

The instrument electronics contained deglitching circuits, operating in the kHz domain, intended to suppress spikes due to the incidence of ionizing particles. Before the flight the deglitchers, tested with a radio-active source, proved to remove more than 80 % of the noise energy carried by the spikes. Possibly the deglitchers were less efficient in rejecting flux-induced "spontaneous" spikes, either because of their different signatures or because of a tendency of this kind of spikes to arrive in close bunches.

Quite likely low-level spiking was the major source of noise in the CPC. Spiking at rates in excess of 1 Hz would not be recognizable as such, due to the narrow pass bands of the instrument electronics. Fig. 5.1 shows some spike statistics which support this hypothesis.

There probably is a physical connection between spiking and responsivity

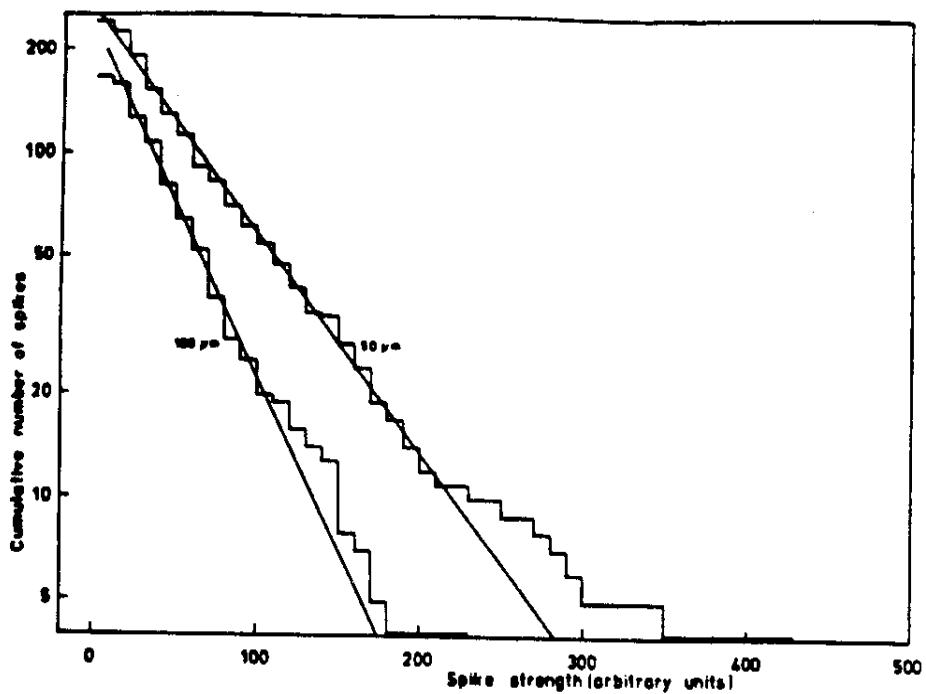


Fig. 5.1. Cumulative number of spikes versus spike strength

These spikes were found by the deglitching algorithm in data on empty fields. Note the excess of strong spikes, and the absence of a cut-off at low values.

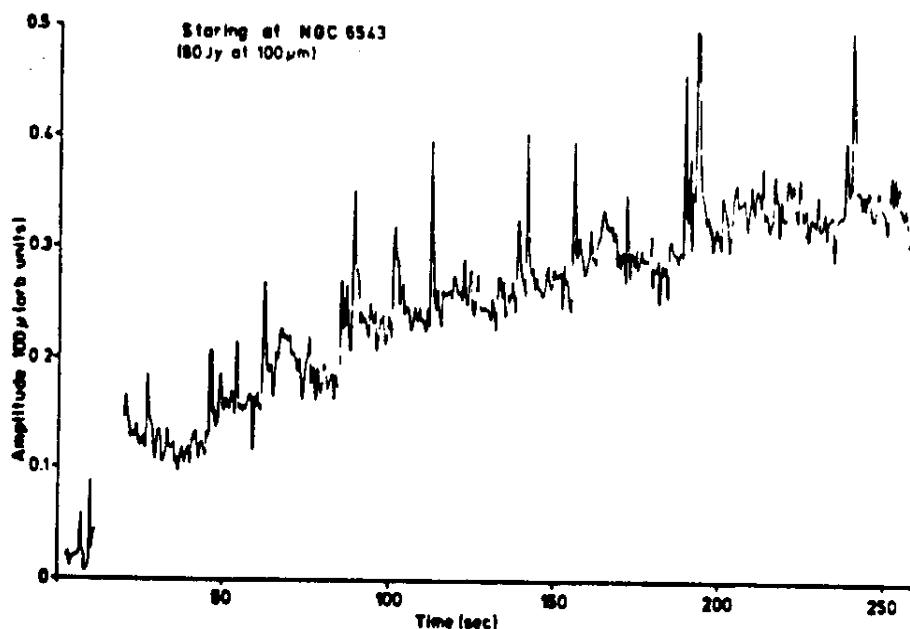


Fig. 5.2. The CPC response during a stare at NGC 6543.

In the first 10 seconds the source was outside the beam. The data have been demodulated but not deglitched. Two effects are evident:

- the response keeps rising until an equilibrium is reached after 200 seconds
- many spikes appear to coincide with instantaneous responsivity increases.

changes. On a rising signal spikes often appear to co-incide with instantaneous responsivity increases; fig. 5.2 provides an example of this phenomenon.

### 5.1.3. Responsivity variations

On sufficiently bright sources, strong variations of the photometer responsivity are observed on time scales ranging from a few seconds to several minutes (the maximum duration of an observation is about 7 minutes). These are strongly non-linear effects, as both the magnitude and the time scale of the variations depend on the previous and present input signal intensity. In extreme cases gain variations by a factor of five have been observed.

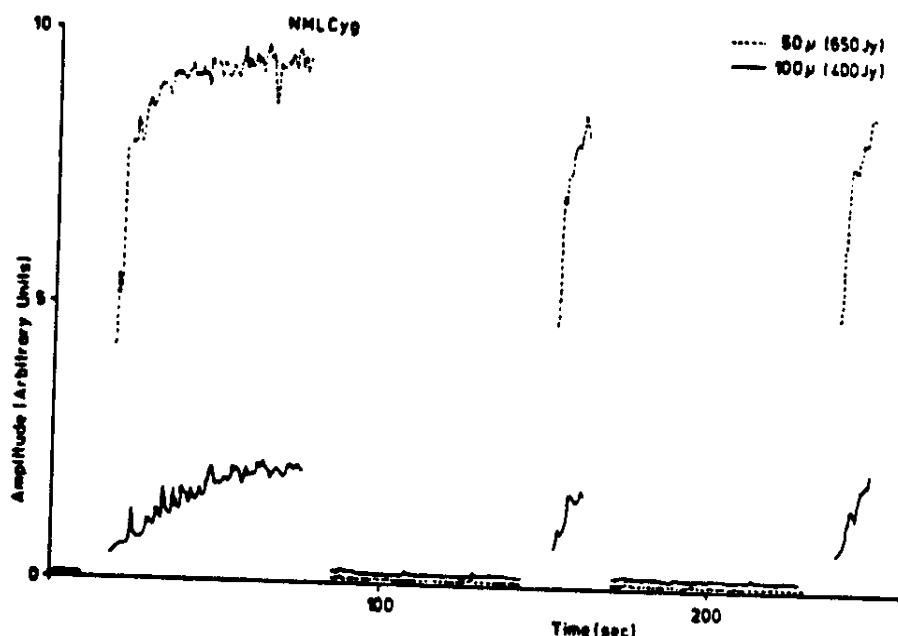


Fig. 5.3. Responses to a strong source (NML Cygni).

The results from three stares on the source, alternated with blank-sky measurements are shown. The transitions from source to sky and back (during which no CPC data were recorded), were sufficiently long for the pointing to stabilize. Raw data have been plotted, after demodulation but before deglitching. At these high signal levels spiking is not predominant. On this very strong source the equilibrium response is obtained after 60 seconds. After a 60-second interruption the responsivity is much reduced but it recovers more rapidly. Weaker sources show much less responsivity variations.

The behaviour is quite complex, but two effects stand out. When a relatively faint point source (about 20 Jy or less) on a low background is moved into the beam, there is a clear signal overshoot, relaxing with a short time constant. This overshoot is usually present in the response to the telescope's internal calibrator (see fig. 5.5). The second effect is a slow responsivity increase, at a rate roughly proportional to the incoming flux, and during a time roughly inversely proportional to this flux. For a constant input an equilibrium state, which depends on the input level, is reached after the detectors have been exposed to about  $10^4$  Jy.sec / arcmin<sup>2</sup>. For exposure levels around 120 Jy/arcmin<sup>2</sup> the responsivity doubles in about 30 sec. The

magnitude of this long-term effect may be as large as a factor 5. A few seconds in darkness are sufficient to lose most of this gain increase, but the high responsivity is recovered very fast if the system has not had enough time to relax.

These effects were recognized as the observing program proceeded. The distortions due to responsivity variations can be very strong, but are quite reproducible. To characterize the effects quantitatively, special calibration observations were performed.

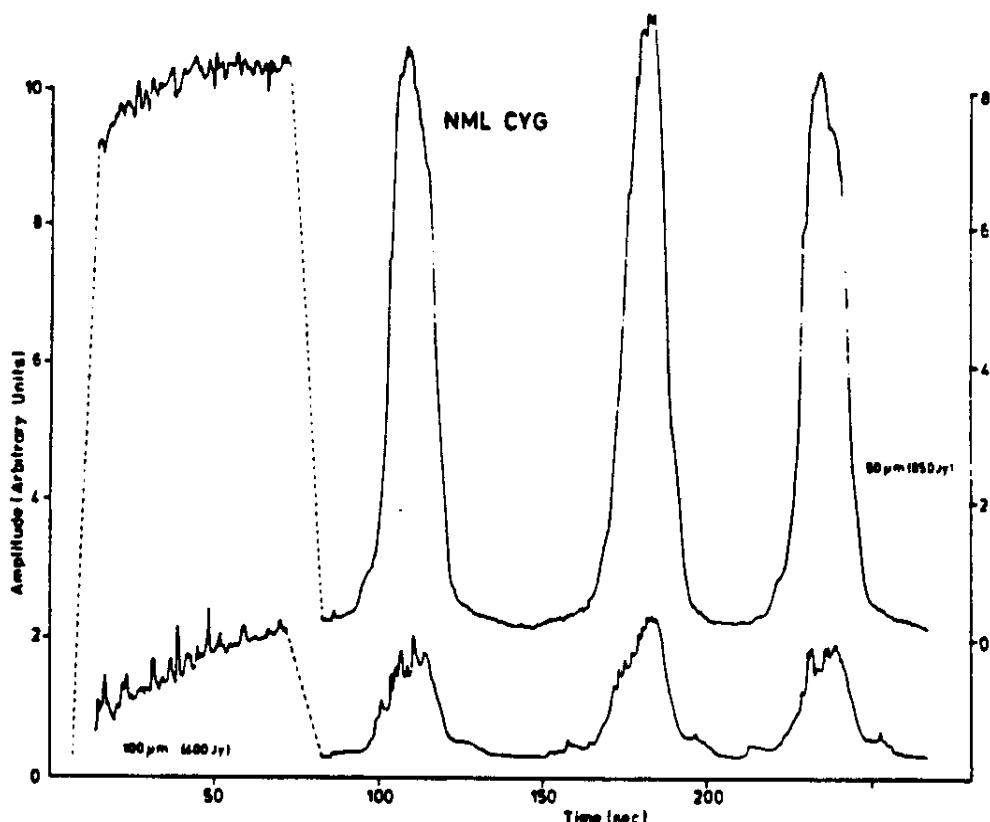
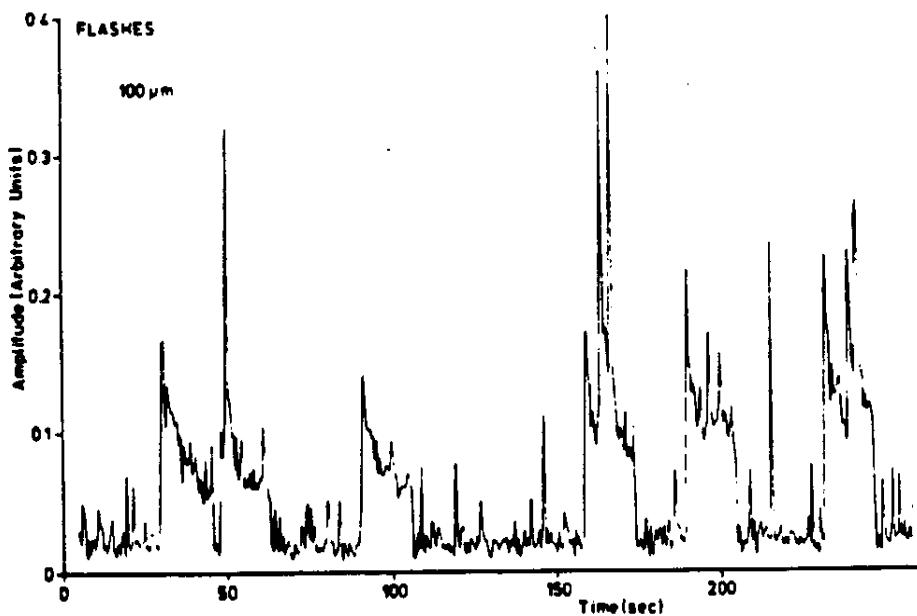
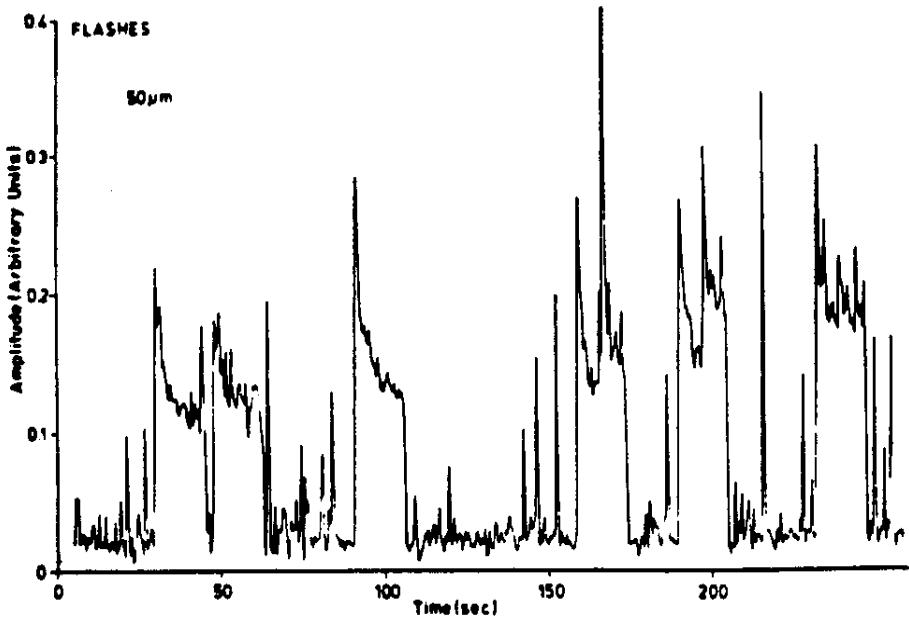


Fig. 5.4. Responses to a strong source (NML Cygni).

The results from a stare on the source, followed by three slow (0.075 arcmin/sec) scans in alternating directions are shown. Raw data have been plotted, after demodulation but before deglitching. The scan direction has a small influence on the response; this must be caused by a leak in one of the two additional CPC apertures meant for a beam-switching mode - radiation through this aperture is not modulated but reaches the detectors.

One set of calibration observations consisted of pointing measurements alternating between a strong or moderately strong source and a low-level background nearby. Each phase lasted between 10 seconds and a few minutes. Unfortunately, operational limitations precluded recording data during the 7 or 8 seconds slew between the two positions. Examples of results from such observations are given in Figures 5.3 and 5.4.



**Fig. 5.5. Response to a sequence of stimulator exposures.**

While pointing at blank sky, the internal stimulator was activated during 6 15-sec intervals, at  $t = 25, 43, 86, 160, 185$  and  $227$  sec. The data were demodulated, but not deglitched.

Each flash response shows an initial signal overshoot, a short-term responsivity variation effect. The overshoot on the second flash, which followed closely on the first one, is less pronounced. A longer-term effect is the response increase from one flash to the next. The spiking is strong, but does not seriously affect the measurement accuracy.

Similar observations have been carried out on a very low background, using the internal calibrator as a source. Fig. 5.5 shows such an observation. The initial signal overshoot is conspicuous, but it appears only after a sufficiently long interruption (the threshold is between 4 and 16 seconds). The integrated exposure is insufficient to show the long-term responsivity increase.

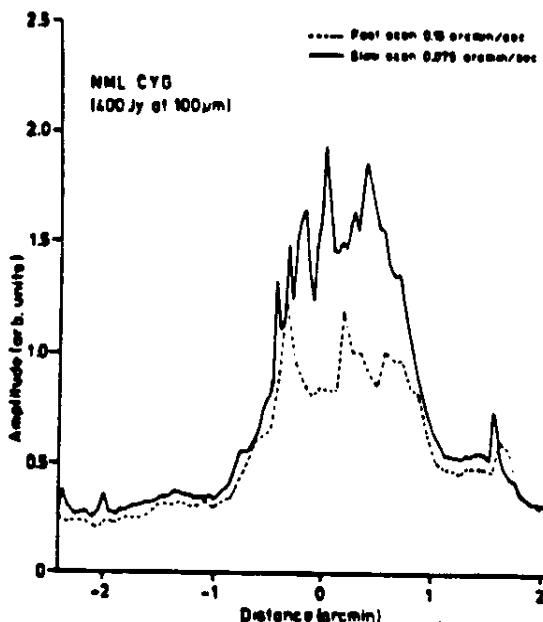


Fig. 5.6. Scan-rate dependence of the response to a strong source (NML Cygni).

Long-term responsivity increases are of course dependent on the scan rate. During a slow source crossing the responsivity build-up can be appreciable. This effect is more pronounced at 100  $\mu\text{m}$  than at 50  $\mu\text{m}$ . It is much less severe for sources of 100 Jy or less.

Repeated scans at various speeds across sources of various brightness show the beam profile distortions resulting from the responsivity variations (Fig. 5.6). The maximum response reached in a fast scan is generally lower than the value obtained after a long integration on the source. The profile is usually asymmetric, and the peak may be shifted forward or backward, due to the overshoot effect or to the long-term effect, depending on the scan speed and on the source intensity.

#### 5.1.4. Attempts at modeling the responsivity variations

The reproducibility of the anomalous gain effects made us hope that we might be able to characterize the detector behaviour sufficiently to enable us to devise a correction procedure. We constructed a phenomenological detector model, described below, that can reproduce the results of the calibration measurements reasonably well. However, using this model to reconstruct the IR signals on the detectors turned out to be impractical, for reasons that are

probably fundamental. In the first place, such a reconstruction process is very sensitive to noise, particularly when superimposed on signal gradients. A second problem is its high sensitivity on the assumed initial state of the detector in terms of model parameters. Finally, the model predicts much too small responsivities at low input signal levels. In view of the inherent instability of a direct correction procedure and of the reasonable agreement between CPC and survey fluxes over a large dynamic range, we decided not to attempt any correction based on a detector model.

In the phenomenological detector model the state of the detector is defined by two quantities, a gain factor  $G$  and a saturation level  $F_s$ . The input signal  $F_{in}$  and the response  $F_{out}$  are related by

$$F_{out} / F_s = 1 - e^{-G \times F_{in} / F_s}$$

The values of both  $G$  and  $F_s$  are variable, controlled by first-order differential equations. The behaviour of  $G$  determines the long-term responsivity variations,  $F_s$  accounts for the short-term effects.

The differential equation for the gain factor is

$$\frac{dG}{dt} = A \times F_{in} \times (G_{max} - G) - B \times (G - G_{min})$$

where the constants  $A$ ,  $B$ ,  $G_{max}$  and  $G_{min}$  are chosen to fit the experimental data.

$G$  tends to an equilibrium value

$$G_{eq} = (A \times F_{in} \times G_{max} + B \times G_{min}) / (A \times F_{in} + B)$$

with a time constant equal to

$$\tau = 1 / (A \times F_{in} + B)$$

An analogous differential equation applies to the saturation level  $F_s$ , with  $F_{in}$  replaced by  $(g \times F_{in})$ .

### 5.1.5. Laboratory tests

Laboratory tests on Ge:Ga detectors from the same supplier failed to reproduce the detector behaviour experienced during the flight. In these tests the electrical configuration and the temperature of the detector and the pre-amplifier were the same as during the flight, while the signal levels were in a range where strong effects have been observed. Signal-related short-term responsivity variations remained below the 5 % level. Stronger gain variations accompanied by spiking were observed occasionally, but only after strong electrical disturbances.

## 5.2. Sensitivity

In this section we will discuss the sensitivity of the CPC observations. The responsivity changes discussed in the previous section affect the sensitivity. The ability to detect point sources depends on the previous signal detection history of a detector. If there is much infrared flux in a map, the ensuing distortions in the infrared image will effectively make the signal to noise worse.

We analyze a few CPC images with relatively little flux. Such low-flux images reasonably well represent the real infrared distribution on the sky, and the noise can be determined quite well. A sizable number of CPC maps fall in this category, e.g. all images obtained outside the galactic plane and the LMC.

We first selected an "empty" image; this one was a large planetary nebula at high galactic latitude, too weak to be detected. A histogram of the surface brightness values can be approximated quite well by a gaussian. The standard deviation of this gaussian,  $B_g$ , is interpreted as the uncertainty in the surface brightness for a single pixel.

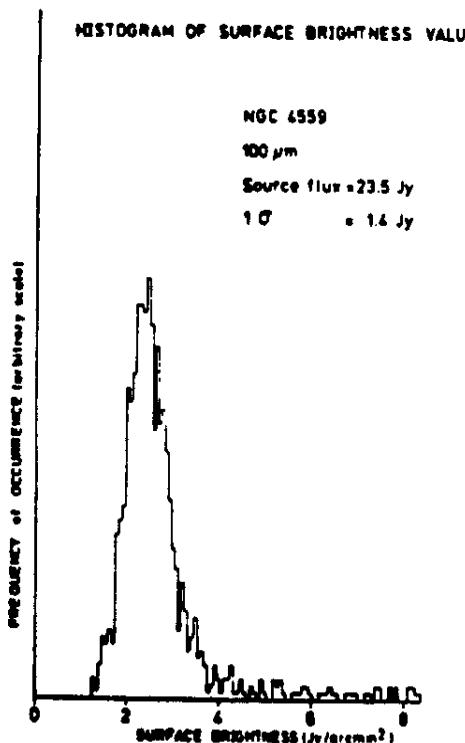


Fig. 5.7. Surface brightness distribution in a map around NGC 4559.

The histogram is dominated by blank-sky samples; the values above about 3.5 Jy per sq.arcmin are due to the source NGC 4559. The noise, although probably dominated by low-level spikes (see fig. 5.1), apparently has a nearly Gaussian distribution.

In images containing relatively little flux the histogram of surface brightness values exhibits also a gaussian shape at the low surface brightness values, with a tail extending to large values. An example is shown in Fig. 5.7;  $B_g$  can be determined quite well.

Table 5.1. Examples of total flux determination.

Source Name	CPC Band ( $\mu\text{m}$ )	Source Flux (Jy)	$B$ (Jy/ $\text{arcmin}^2$ )
Empty Field	50	0.6	0.3
NGC 4559	100	0.9	0.4
	50	3.4	0.3
NGC 1961	100	23.5	0.4
	50	10.1	0.4
M 81	100	50.6	0.5
	50	13.0	0.5
	100	33.9	0.7

Even for images containing not too much flux spread out over the image,  $B$  can be determined. E.g. for the image of M 81 the histogram is too skewed to be represented by a gaussian. By using only the part left of the maximum, which does resemble a half-gaussian,  $B$  can be estimated reasonably well, and it is only slightly larger than the empty map noise.

Converting  $B$  into an uncertainty estimate for total flux determinations (e.g. to use as a point source detection limit) is not straightforward, because the regridding process causes the noise in adjacent pixels to be correlated, in a way that depends on the exact scan path for the observation.

We used the procedure outlined in sections 8.2 to determine the fluxes of a number of weak sources (see table 5.1). The result on an empty field, or on an empty area in the map, is indicative of the reliability of the so determined fluxes. Fluxes down to a level of a few Jy can be determined.

### 5.3. Observed beam profile

Knowledge of the CPC beam profiles can serve at least three purposes:

- to estimate the extent of an isolated source,
- to separate sources lying very close to each other,
- to determine the flux of an isolated point source from its peak surface brightness.

Note that the beam profile plays no role in the photometric calibration of the instrument; all maps are given in terms of surface brightness, and fluxes of sources can be found by integrating their surface brightness.

Determining the beam profiles observationally requires a true point source sufficiently bright at the CPC wavelengths. There exist very few sources that meet these requirements; most bright 50 and 100  $\mu\text{m}$  sources have extents that are significant compared to the 1.2 arcmin diameter of the CPC's entrance aperture. The asteroid Ceres was selected for this purpose; at the time of observation its flux was 200 and 105 Jy at 50 and 100  $\mu\text{m}$ , and its diameter about one arcsec. We obtained 8  $9 \times 12$  arcmin maps of Ceres; the results of the observations are summarized in Table 5.2. To characterize a profile width, we use the effective solid angle of the profile, i.e. the total

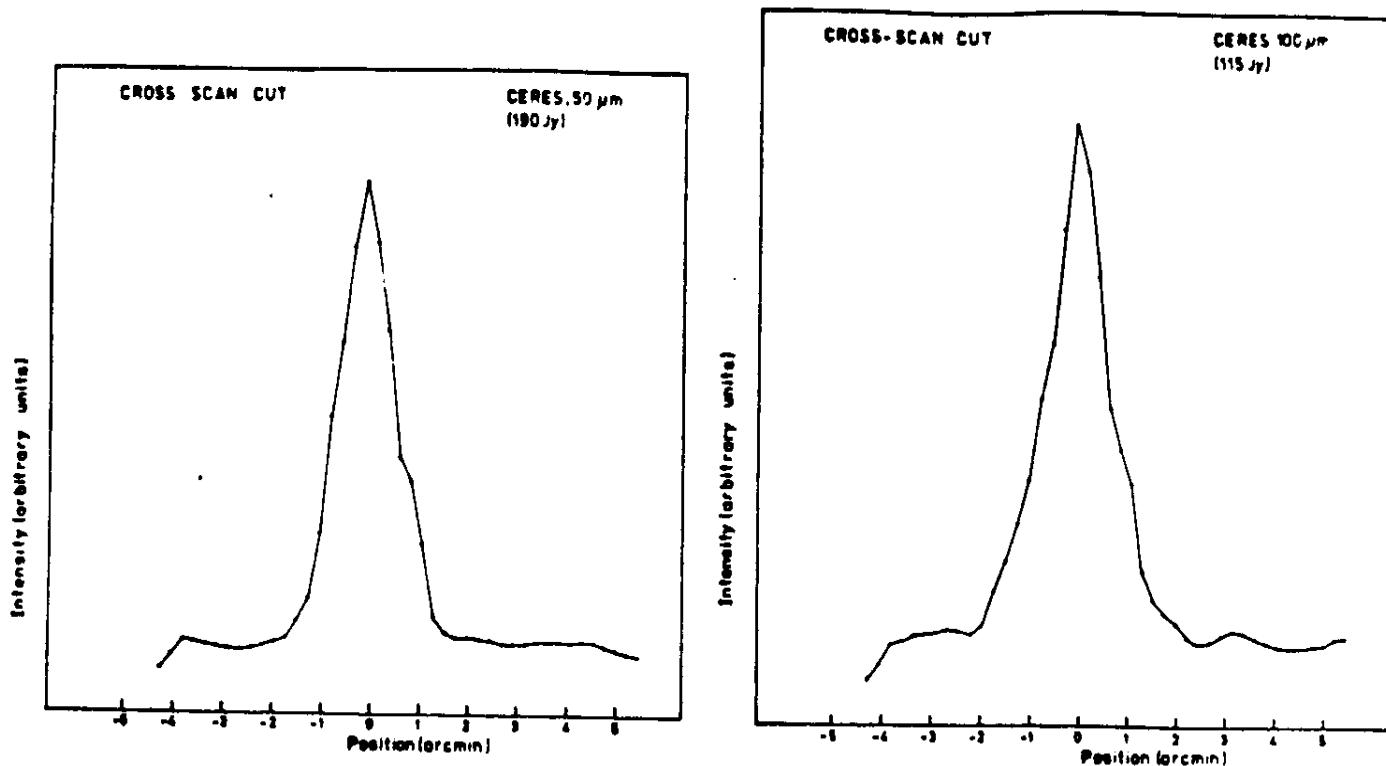


Fig. 5.8. Observed beam profile

Cross-scan cuts through images of Ceres at 50 and 100  $\mu\text{m}$  are shown (a CPC09A observation, see table 2.1). The FWHM at 50 and 100  $\mu\text{m}$  is 1.4 and 1.6 arcmin respectively. Average values from all Ceres observations are presented in Table 5.2.

flux divided by the peak surface brightness, and the full width at half maximum (FWHM). Figure 5.8 shows cross-scan cuts through the best image of Ceres.

Table 5.2. Beam characteristics from observations of Ceres		
The quoted uncertainty is the r.m.s. deviation of a single observation from the mean.		
Band	Solid Angle (arcmin $^2$ )	FWHM (arc sec)
50 $\mu\text{m}$	$2.5 \pm 0.2$	$88 \pm 4$
100 $\mu\text{m}$	$3.3 \pm 0.2$	$100 \pm 3$

The internal consistency of the Ceres measurements is somewhat misleading; the observed short-term responsivity variations (see section 5.1) cause flux-dependent distortions of the source profiles. This might explain the inconsistency of the results on Ceres with the theoretical beam profile (section 7.4).

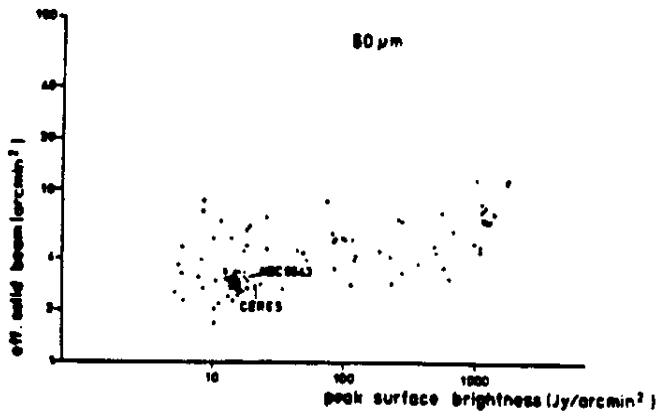
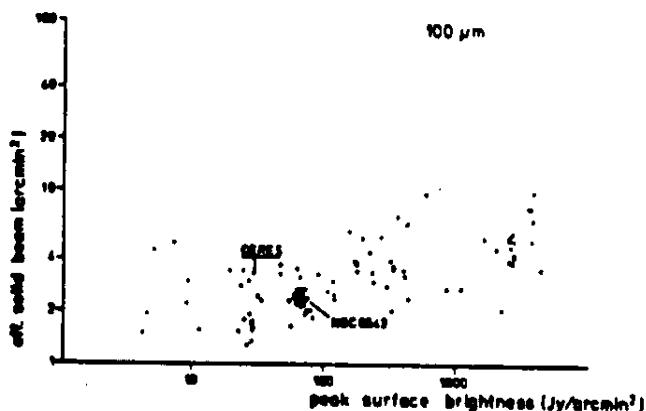


Fig. 5.9. Peak surface brightness and flux density

These figures show the effective solid beam (the ratio of measured flux density and measured peak surface brightness) and the peak brightness for a number of point sources. The scatter indicates that peak brightness is an unreliable indicator of source strength. The slight tendency of the effective solid beam to increase with source flux is undoubtedly caused by short-term responsivity variations.



Indeed when we compare the Ceres observations with other observations of likely point sources, we do find a correlation of the apparent width of the beam profile with the source peak surface brightness. Figure 5.9 shows the results of the comparison. In producing these data we needed a scheme to estimate the background in a map; for this purpose we used the median value of the surface brightness (cf. section 5.2). The apparent beam size tends to increase with the source brightness, but there is an appreciable scatter. One cause for this scatter is undoubtedly that the background surface brightness also influences the responsivity variations.

The main conclusion from the beam profile measurements must be that great caution is required in interpreting the extent of sources in the CPC maps. Also, peak brightness is an unreliable basis for a flux estimate; the photometric calibration of the CPC is based on integrated fluxes.

## 6. Data reduction

### 6.1. Input data base

The CPC images were produced from a data base set up during the mission at the ground station. The contents of this data base are as follows:

- a complete log of the observational schedule;
- assorted satellite data not transmitted in the high-speed telemetry, notably the results of the attitude calibration measurements;
- alignment and calibration parameters of the satellite attitude system;
- satellite board clock calibration;
- status of telemetry quality;
- for the whole period covered by the telemetry from the satellite, once per second the status of the DAX instrument (temperatures, voltages etc.);
- the CPC 64-Hz digital data, for the periods the satellite was commanded to CPC data handling.

About three hours after the completion of each 12-hour observing period (SOP), a tape containing these data in 6 files, was delivered to a ROG crew at the ground station. The contents of this tape were then immediately processed for data quality verification, quick-look reduction and archiving (combining several SOP's worth of data to a single tape). The total comprises about 800 MBytes of data on 32 tape volumes.

### 6.2. System design

The software system for production of the CPC images is designed around two special file formats, DAX files and image files. The different steps in the reduction are performed by about half a dozen programs which repeatedly process files in these formats. The relation between programs and files is shown in Fig. 6.1.

Both file formats were designed to contain a complete subset of the data base, in the sense that all the relevant information for processing was present in each file. This avoided the construction and maintenance of auxiliary data bases, at the cost of about 10 % overhead in file size, due to the presence of multiple copies of global information structures. Also some derived quantities had to be recomputed for each file anew, instead of being globally available. The main profit of this setup was the production flexibility. For all reduction steps we could choose a compromise method between two extremes. At one end we could run large volumes of data in batches through a single program and store the intermediate results, at the other end we could generate a single observation end product by running a single file through all programs in a pipeline connection.

The DAX file is capable of holding all data pertinent to a few observations, usually the 12-hour operational period (SOP) is kept together. The

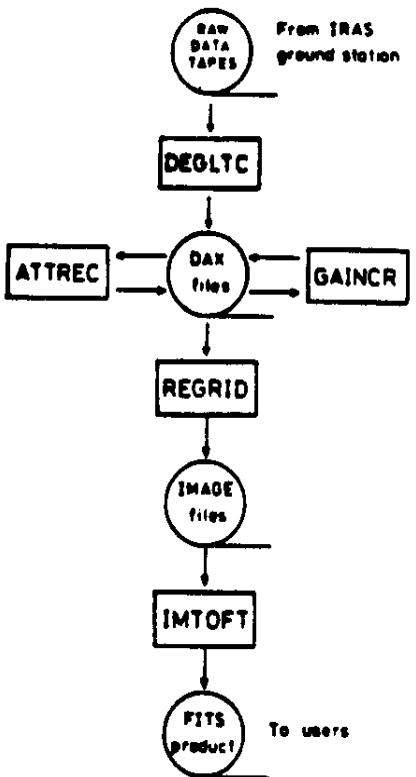


Fig. 6.1. Schematic data flow of the CPC reduction system.

See text for a description of the various parts.

data are maintained in time order in an intermediate stage of reduction, while various programs derive and add calibration parameters without changing the DAX-file format. This setup enabled us, at least to a certain extent, to exchange the order in which some programs operated on the DAX files, or even to reprocess DAX files without having to regenerate an intermediate product.

The image files are used for the intermediate reduction stage where the time order is lost and the results are stored as images, i.e. estimated surface brightness values at a regular grid on the sky. Each image file contains the data for one observation.

### 6.3. Demodulation and deglitching

The first program in the reduction scheme is DEGLTC, which creates a DAX file for one SOP from the data tapes received from the ground station. The data are processed by DEGLTC in three steps.

- a. The consistency of the input files is verified and the DAX-file format is set up.
- b. The digital data stream of the CPC is decompressed. The 64 samples per second of the detector output values are reconstructed from the digital 8-bit data stream by table lookup. Demodulation is done by correlating 8 consecutive samples with a sine function at the known fixed chopping frequency of 15.062 Hz, with the phase as free parameter. This resulted in 8 samples of modulation amplitude per second per detector.
- c. To suppress the spiking behaviour of the detectors, a deglitching algorithm is applied to the 8-Hz data, independently for each detector. The deglitching algorithm recognizes spikes by a sudden increase in response,

followed by a decrease to the original level on a time scale of 0.5 seconds. When a spike is detected the estimated amplitude of the spike is subtracted. Both the deglitched data stream and the original 8-Hz data stream are then smoothed by averaging over half-second intervals. The resulting two values per second are stored in the DAX file for further processing.

Side effects of the demodulation and despiking methods are discussed in section 7.1, a detailed description of the algorithm is given in Annex 1.

#### 6.4. Responsivity variation

Correction for gradual changes in detector responsivity ("gain") during the observation is done by the program GAINCR, usually the third step in the reduction process. The algorithm is based upon the following assumptions.

- The demodulated and deglitched response of the detector is equal to observed sky surface brightness multiplied by a gain function.
- The gain changes slowly in time, on time scales comparable to the duration of a leg of the raster scan.
- In the part of the sky covered by the raster scan, a background region of constant surface brightness is present, crossing the scan legs, thereby providing a reference level that is observed several times during the observation.

After selecting a number of samples representative for the background, the change observed in this background is modelled and used to derive the gain function. The instrumental causes of the gain variations are described in section 5.1, the validity of the correction method is discussed in section 7.2.

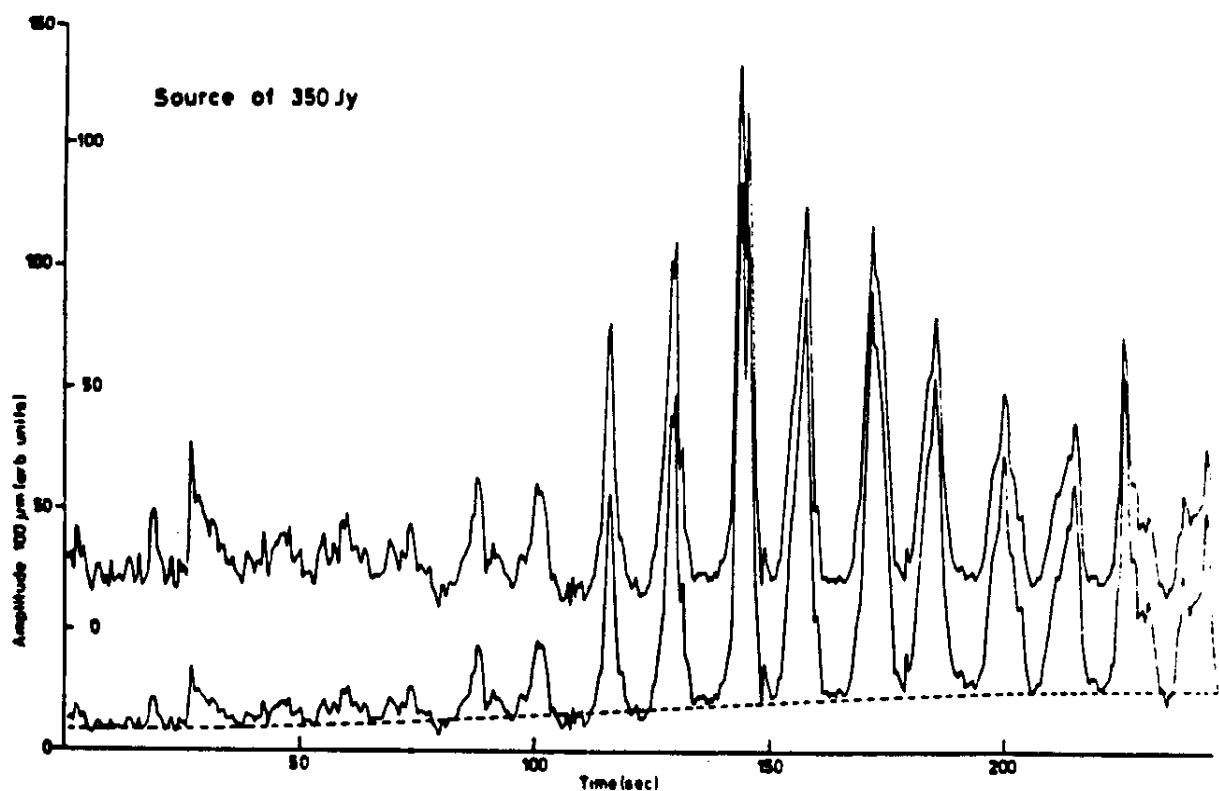
The background region is determined by taking the despiked response values for one detector as a function of time from the input DAX file, two values per second of observation. The lowest values from each pair of legs are selected as background samples, until the summed response in the selected points reaches a value of 1 Instrumental Unit ( $\sim 100 \text{ Jy/arcmin}^2$ ), or until 20 points in this pair of legs are chosen.

The gain variation is then modelled by fitting polynomials of degree 0 to 4 through the response values in the background region (see Fig. 6.2). The residual variances of these fits are compared, and if two polynomials have a difference of less than 20%, the higher-order one is rejected as being unnecessarily complex. The remaining polynomial with the highest order is considered to model the gain variations.

Finally the gain function is determined by normalizing the gain variation polynomial so that its value for the maximum response in the whole map is equal to one. The despiked data values are then divided by the gain function for that detector, while the 'raw' data values are unchanged. The resulting data stream is stored in the same DAX file format as the input data.

The gain correction procedure was considered to be dubious when one or more of the following cases applied.

- There is no clearly recognizable background region: less than 10 % of the



**Fig. 6.2. Long-term responsivity variation correction**

The lower plot shows the original observation: the background increases slowly due to the long-term increase in gain. The background was fitted by a function represented by the dashed line. The gain function is normalized at the peak (at about 145 sec) and the resultant plot is the higher one (shifted upward for sake of clarity).

samples in the whole map are selected as belonging to the background.

- The minimum and maximum values of the gain variation have a ratio of 6 or more.
- A  $\chi^2$  test reveals that the response variations on the background cannot be fitted by the chosen gain variation polynomial. The  $\chi^2$  test uses the mean absolute difference between successive samples in the whole map as an estimate of the standard deviation  $\sigma$ . The fit is rejected whenever  $\chi^2$  exceeds the 0.1 % probability limits meaning that of the cases where the model was valid, 1 in 1000 will be falsely rejected.

A dubious gain correction at either wavelength is taken to affect the whole observation; a remark is then added to the output file, which will prevent the appearance of this observation in the current end products.

### 6.5. Pointing reconstruction and regridding

The program ATTREC reconstructs the viewing direction of the CPC hole at the sky from the satellite attitude information:

- a. the satellite position as commanded by the ground station,
- b. the servo error (difference between commanded and observed position) as used in the attitude servo loop and reported back by the satellite,

- c. an inversion of the algorithm used by the ground station to convert celestial coordinates to satellite position commands,
- d. the slow changes in the attitude control system as measured and reported by the satellite upon execution of an attitude calibration scan.

The conversion of satellite position commands to celestial coordinates needs the position of the sun, which is assumed constant for the duration of the raster scan. It is computed for the time halfway the raster according to the prescriptions of Newcomb (1895) to about 1 arcsec accuracy. For the misalignment parameters which describe the viewing direction of the CPC hole with respect to the satellite attitude control coordinate frame, we use the nominal values provided by the ground station for the optical axis of the telescope, with a fixed correction for the relative position of the CPC hole.

The attitude calibration measurements were used to determine the mispointing of the attitude system by scanning special visual sensors over a star with known position. During the CPC raster scans, the onboard software corrected the commanded attitude for difference between achieved and intended viewing direction as computed from the last successfully executed attitude calibration scan. The reconstruction, done in ATTREC with the originally commanded attitude in combination with the nominal misalignments, amounts to using the misalignments actually valid at this latest attitude calibration. Routinely, attitude calibration scans were requested before and after each CPC raster scan.

The second attitude calibration, done after the raster scan and the flux calibration measurement, was used to determine the change in misalignment correction. The change was usually negligible in the cross-scan direction, being the mechanical misalignment between the sun sensor and the telescope. In the in-scan direction the change is mainly caused by the error in the integration of the gyro readouts. This occurred chiefly during the slew manoeuvres (e.g. going from the attitude calibration track to the raster scan). The change in misalignment between the two attitude calibrations is interpolated by ATTREC in proportion to the number of slews performed, and assumed constant during the raster scan.

The reconstruction of the raster scans uses an in-map coordinate system. The axes of this system coincide with the in-scan and cross-scan directions. The origin of the in-map coordinates is established by determining the commanded sky position for a sample halfway the middle leg, and rounding the result to a point on a predetermined 1 arcminute grid in RA/Dec. The rounding to a fixed grid facilitates superposition of overlapping maps. Right ascension, declination of the origin of the in-map coordinate, and position angle system are recorded in the DAX-file.

For each leg of the raster scan the commanded positions of the first and last sample on the in-map coordinate system are computed and stored. The servo errors, giving the recorded deviations from the commanded scan are already stored in the DAX-files on a one-second basis.

The program REGRID computes the sky surface brightness at a regular pixel grid. In doing so, the information is converted from the time domain to the image domain, the result is of necessity in a different format. The grid is always at 20-arcsec pixel size, oriented in RA/Dec, with the center position

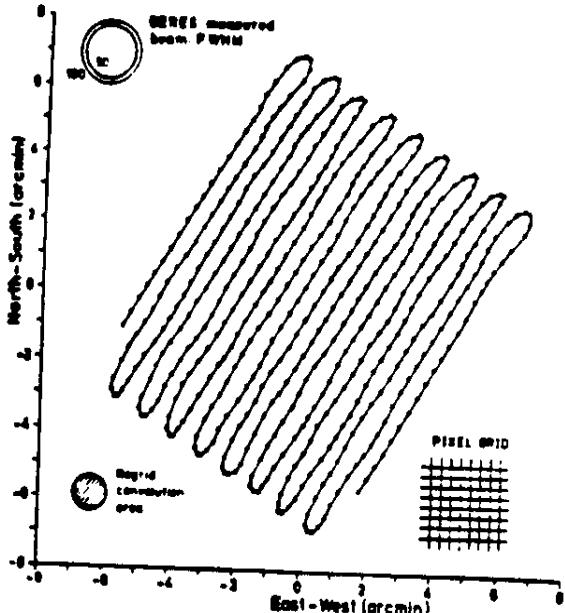


Fig.6.3. Movement of CPC diaphragm over the sky during a CPCF9A raster scan.

The scan starts in the lower left corner. Dots indicate the viewing direction at half-second intervals. For comparison, the FWHM observed beam diameter, the convolution diameter used in regridding, and the pixel grid size are shown.

at the origin of the in-map coordinate system. Correcting the reconstructed commanded position with the control errors, both available at one-second intervals, gives the actual track of the CPC diaphragm over this grid.

By quadratic interpolation a position is assigned to each half-second surface-brightness sample. The surface brightness at each pixel of the grid is computed as the average of all samples that are within 32 arc seconds of the pixel position. This amounts to a convolution of the data by a circular beam of the same radius and rectangular cross section. The surface brightness is considered undefined for pixels where no sample is taken within the 32 arc second radius. The procedure is (partly) depicted in Fig. 6.3.

A conventional astronomical object name, usually provided by the requester of the observation, is added from a manually maintained list, as an aid in identification.

## 6.6. Calibration and generation of end products

Program IMTOFT is the final step in the reduction process, reformatting the regredded images to FITS format. The surface brightness  $B_{int}$  is kept in internal units up to this stage, where it is converted to  $B_{stnd}$  in MJy/ster. The overall calibration factor  $A$  and the sensitivity change time scale  $T$ , derived in sections 8.1 and 8.2, are given in table 6.1. The conversion applicable at the time of observation  $t$  (in years) is then given by the formula:

$$B_{stnd} = \frac{A}{1 - (t-1983.0)/T} \times B_{int}$$

In order to make the difference between 'clean' and 'raw' images (see section 3) visible, a margin is added to the images, which is filled with undefined data values for clean images. For the raw images the margin contains

Table 6.1.  
Calibration of instrumental units.

Wavelength $\lambda$ ( $\mu\text{m}$ )	Calibration Factor (Jy/arcmin $^2$ per I.U.)	Calibration Factor (Jy/pixel $^A$ per I.U.)	Timescale $T$ (year)
50	70	7.8	3.5
100	105	11.7	3.0

the character pattern 'RAW IMAGE' (or the part of it which fits).

When finally preparing the tape, dubious observations as described in the previous sections, are prevented to appear in the current product. Each file on the resulting FITS tape contains two images at 50 and 100  $\mu\text{m}$ , stored as two planes in a three-dimensional data array. The clean and raw images are paired as two files of identical size, and the observations are sorted to Right Ascension.

The FITS header section is built upon a rather rigid template, where only the values needed for a quantitative interpretation of the data are given as FITS keyword parameters:

- type, amount and organization of the data on tape,
- scale of the maps and position on the sky,
- calibration of the FITS tape values to MJy/ster,
- epoch of observation and of tape generation.

Other parameters, which assist in a qualitative interpretation, are passed in COMMENT fields. If numeric values appear in comment positions, they must not be used for detailed computations. E.g. we give the beam position for the first and 10th second only to convey an impression of the execution of the raster scan.

## 7. Analysis of reduction techniques

### 7.1. Demodulation and deglitching

The potential side effects of the chosen demodulation technique result from the choice of ignoring the phase information. This can reduce the measurement accuracy at signal-to-noise ratios of order 1 or less; at such low signal levels the noise tends to get rectified and thus adds to the amplitude estimates, and any sign reversals in the modulation remain undetected. In a number of test cases we computed the phase for each 8-Hz demodulation interval. This showed that, apart from a systematic influence of the signal level and except on strong glitches, the phase is quite stable, even at the lowest signal levels. In other words, the 15 Hz modulation is always present with a relatively high signal-to-noise ratio and taking account of the phases would not significantly affect the results. Strong glitches are rectified and therefore systematically over-estimated, but do not pass the deglitching process anyhow. The results of the quick-look processing of CPC data, which employed phase-sensitive demodulation at 2 Hz without deglitching, confirm the conclusion that the phase information in the CPC data is irrelevant.

### 7.2. Responsivity variation

As explained in section 5.1, it is quite difficult to reconstruct the gain variations of the CPC detectors. When the gain drops to a low value, reconstruction of the corresponding surface brightness means dividing the response by a number close to zero, with disastrous effects on the result. This prevented us from applying the model given in section 5.1, instead we 'measured' the gain variations by fitting a smooth function to the background of each observation (section 6.4). As the method searches for a minimum response on each pair of scan legs, it relies on the existence of an area of constant surface brightness crossing the scan legs. This assumption is all right for relatively isolated objects.

When an area with extended emission is observed, the gain variation can not be disentangled from the true background variations. The gain as 'measured' on the lowest values of each leg pair, will then not reflect the true gain variation. Because we normalize the gain to be unity at the maximum response, the effects are limited in the cases where a relatively bright source was observed on a low but non-constant background. The major effect on the resulting map is then a pseudo-background strip, oriented across the scan legs, where the surface brightness is forced to be constant. For relatively weak sources embedded in complex emission structures, the gain variation becomes almost impossible to reconstruct. Annex 2 discusses in detail a few good and bad cases of our gain correction method.

### 7.3. Attitude reconstruction and regridding

Each step in the attitude reconstruction can conceptually be assigned to one of two levels. The first level deals with the local geometry of the executed raster pattern ; the second level deals with the location and the orientation of the raster on the sky.

At the local level, which determines the relative positions in the map, the dominant error stems from neglecting changes in the attitude control system parameters during the raster scan. A slow, linear drift in these parameters would cause scale errors or shear in the map. From the consistency in the attitude calibrations bracketing most CPC observations, we conclude that such distortions will not exceed 5 arc seconds. Although the executed scanning rasters have significant irregularities, particularly near the transitions between scan tracks, the relative attitude reconstruction enables the use of all photometric samples in the regridding process.

At the second level, where absolute positions are determined, the main error is again related to the uncertainty in the attitude system parameters. The special attitude calibration scans with the visual star sensors, bracketing the raster scan, usually provide a net value for the in- and cross-scan errors at the moment of the star sightings. The attitude reconstruction algorithm uses a fixed fraction of the difference between the two values to compensate for drift in the system parameters, but it is not clear whether this is the best procedure. From tests on known objects (see section 2.2) we find that the absolute position error is about 25 arc sec r.m.s..

The input data of the regridding routine is a time sequence of brightness measurements at intervals of 0.5 seconds. With the results of the pointing reconstruction the regular one-dimensional temporal grid is translated into a slightly irregular two-dimensional spatial lattice. The separation of the lattice points is typically 25 arc sec, 30 % of the beam diameter, so that the sky brightness is always adequately sampled.

The regridding routine transforms a map to a regular lattice with a spacing of 20 arc sec. The interpolation algorithm simply assigns to each lattice point the mean brightness measured at all points of the original grid within 30 arc sec. If the original grid were regular, the interpolation would amount to a two-dimensional convolution with a "pill box" function. From this point of view, significant irregularities are found only at the edges of the observed fields; everywhere else proper spatial convolution occurs. As is demonstrated in the next section, the employed interpolation function combines well with the optical beam profile.

### 7.4. Resultant Beam Profile

Accurately known significant contributors to the over-all beam profile applicable to the CPC maps are :

- diffraction at the telescope aperture,
- the CPC aperture geometry,

- telescope motions during the 0.5-second integration time,
- the regridding algorithm.

Imaging defects are unlikely to have played a significant role. The Low-Resolution Spectrometer, housed in the same instrument package as the CPC, requires much higher optical quality and its results gave no evidence of any optical defects (the spectrometer employed a 15-arcsec slit and operated at wavelengths down to 8  $\mu\text{m}$ ). The relay optics in the CPC that image the telescope focal plane onto the entrance stop are simple and not critical.

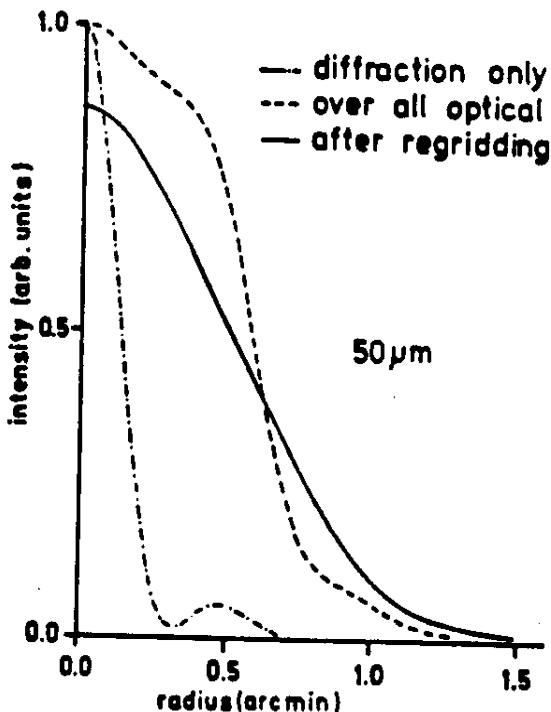


Fig. 7.1. Theoretical beam profile in the 50  $\mu\text{m}$  band.

The optical beams at the telescope focal plane, with and without the effect of the finite CPC aperture are also shown. The over-all optical profile and the profile after regridding have been normalized to the same two-dimensional profile integral.

In practice the beam profile can be distorted by short-term responsivity variations. The most noticeable effects can occur on strong sources, particularly in combination with high backgrounds. At low scan rates the gain increase on strong sources can stretch the source image in the scanning direction; a high background underneath a strong point source can be amplified locally to produce the semblance of wings, again extending in the scanning direction. Probably because of such non-linear effects, the point-source profiles in the obtained maps are often broader than the predicted beam profile.

Figure 7.1 shows the predicted CPC beam profile at 50  $\mu\text{m}$ . To indicate the importance of the various contributors, the figure also shows the Airy function representing the telescope diffraction, averaged over the wavelength band, and the optical beam profile, which is the convolution of the Airy function with the CPC aperture function. After regridding, the profile has a nearly Gaussian shape. The regridding does not change the half-width of the profile and reduces the peak response to a point source by only 13% (optical and over-all profiles are shown on the same scale). At 100  $\mu\text{m}$ , the Airy function is twice as broad and the optical profile is much smoother; the effects of the regridding on profile width and contrast are quite similar.

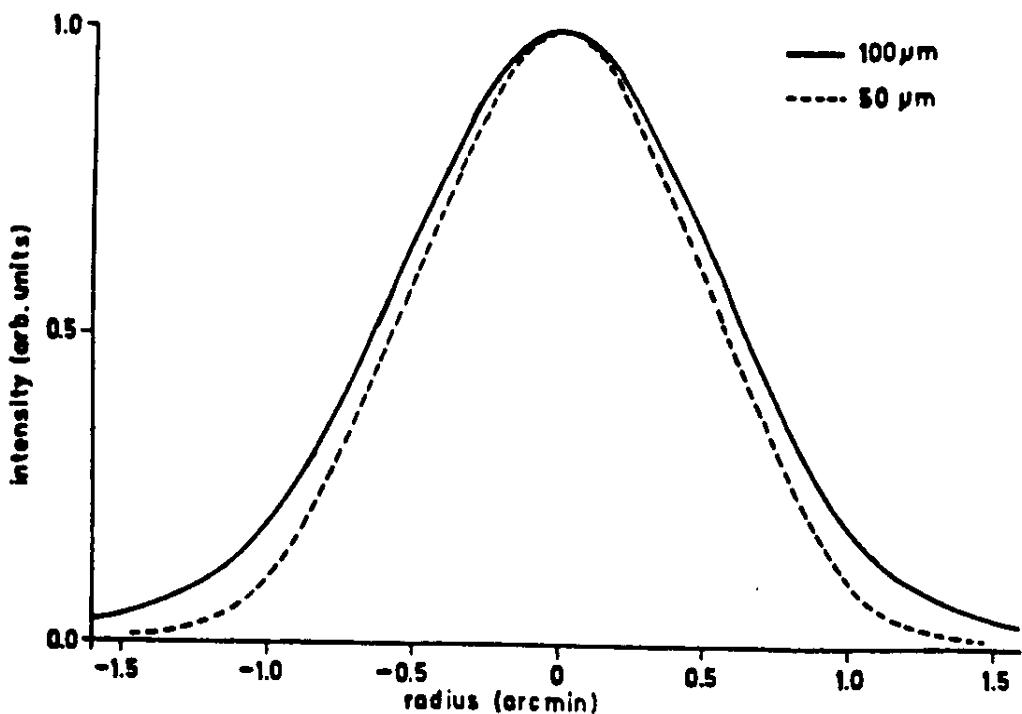


Fig. 7.2. Theoretical beam profiles at 50 and 100  $\mu\text{m}$ .

For the fastest raster scans (CPCF9A macro) an additional in-scan broadening by 3 % is predicted.

Figure 7.2 shows the over-all beam profiles for both CPC channels, normalized to unity peak amplitude.

The figures do not show the additional smoothing in the scan direction due to the finite integration time. At the highest scan rates, in the CPCF9A observations, an in-scan broadening of the profile by only 3 % is predicted.

## 8. Photometric calibration

For the photometric calibration of the CPC observations we used three sets of observations.

- After each CPC observation the "internal stimulator" in the IRAS telescope was used to produce a 15-second long stimulus signal, thus serving as an internal calibrator. The short-term responsivity variations prevented the use of these measurements to calibrate individual observations, but they served to monitor the long-term responsivity changes.
- The planetary nebula NGC 6543, which was used as a photometric reference for the survey instrument, was observed daily with the CPC. These measurements also monitor the long-term responsivity changes, allow a direct assessment of the repeatability of the observations, and firm-up the absolute calibration.
- A large number of point sources were observed both with the survey instrument and with the CPC. These observations provide a check on the linearity of the CPC brightness scale, allow an estimate of the reliability of CPC fluxes, and provide a tie-in with the survey observations. The results of this comparison did play a role in choosing the normalization procedure in the routine used to reduce the effects of signal-induced responsivity variations.

We have no absolute calibration of background levels. To arrive at a meaningful calibration we would need a much better model of the responsivity variations than we can distill from the available material. The widely different beam sizes of CPC and survey array prevent us from using the survey calibration for this purpose.

### 8.1. Sensitivity changes and repeatability

#### 8.1.1. Internal stimulator

We study in this section "flashes" of 15 seconds duration observed after each scientific and calibration observation of CPC. From the response of the survey detectors we know that the flash intensity was constant to a few percent during the whole IRAS mission. Thus flashes seem ideal to establish the absolute level of each CPC observation. This is not feasible because the responsivity variation (described in section 5.1) makes the tie-in of the CPC response to a flash and to an astronomical object uncertain due to the time lag of at least 30 seconds (on average a few minutes). In addition, on high backgrounds the signal-to-noise ratio of the flash response is low. In spite of these problems the flash response as a function of time can be used to study long-term responsivity changes of the CPC detectors.

In Fig. 8.1 we show the flash intensity versus time for 829 flashes. The routine flash measurement consisted of 8 seconds background, 15 seconds stimulator on, 7 seconds background. The response of the detectors on the stimulator is shown in Fig. 5.5. Note the predominance of flux-induced spikes; the software deglitcher was not used on these measurements. As a measure of the flash amplitude the difference between the medians of the stimulator and background samples is used, to minimize the influence of spikes.

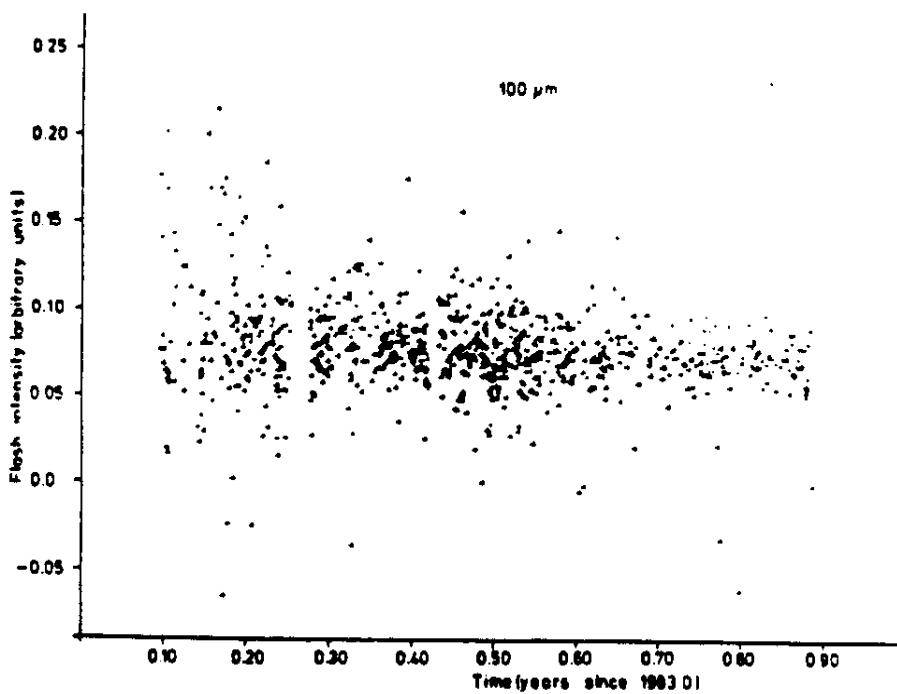
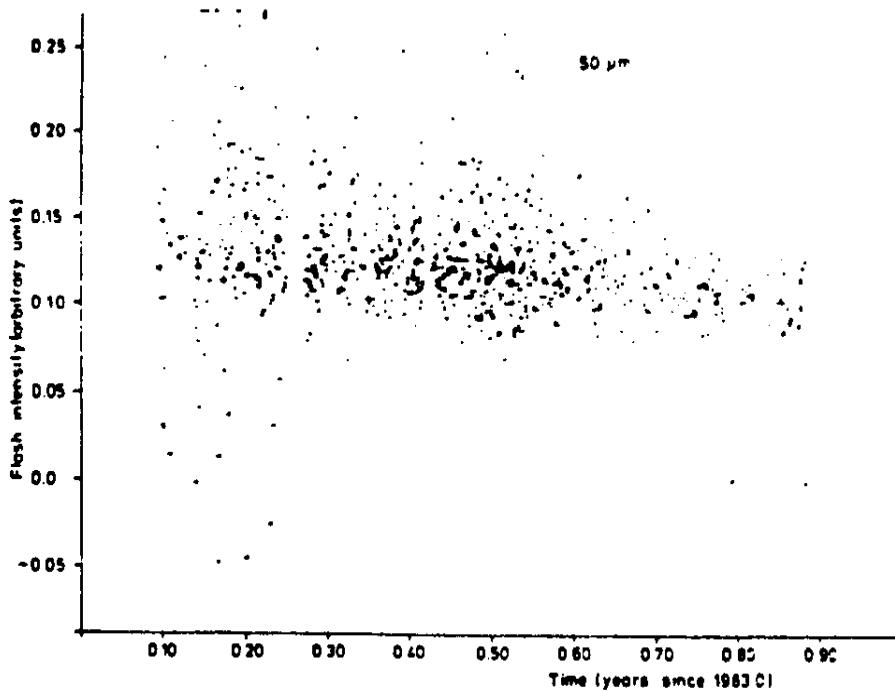


Fig. 8.1. Photometric stability and repeatability, from internal calibrations.

The results of several hundred measurements on the internal stimulator are plotted in this figure. The spread is considerable: about 25 % r.m.s. The slight downward trend is consistent with results obtained on NGC 6543. The mean stimulator signal corresponds to the peak signal from a point source of 21 or 26 Jy at 50 or 100  $\mu$ m respectively.

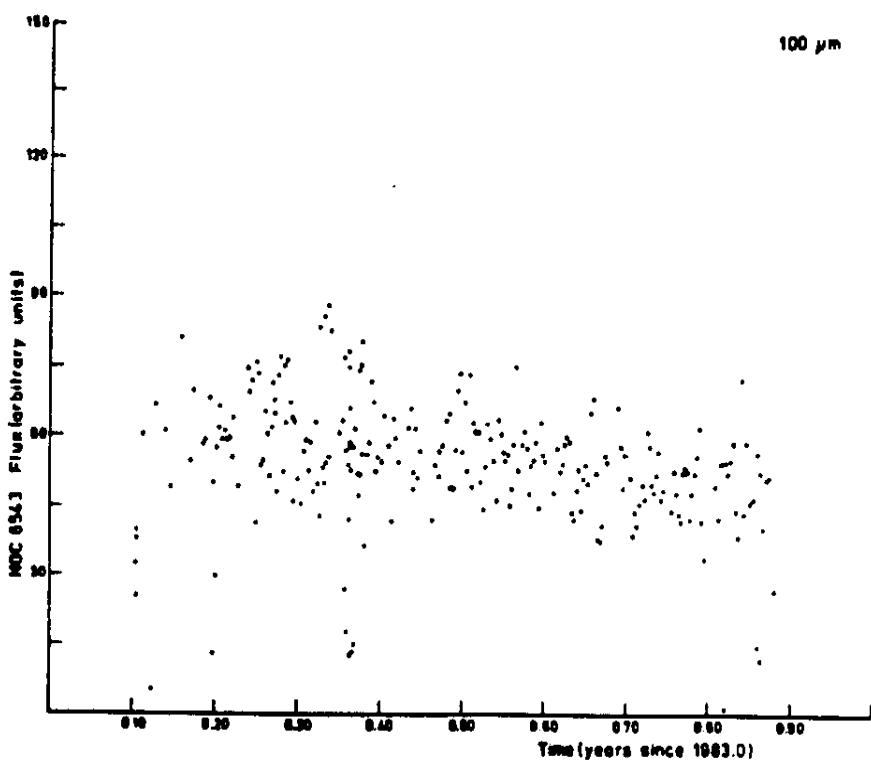
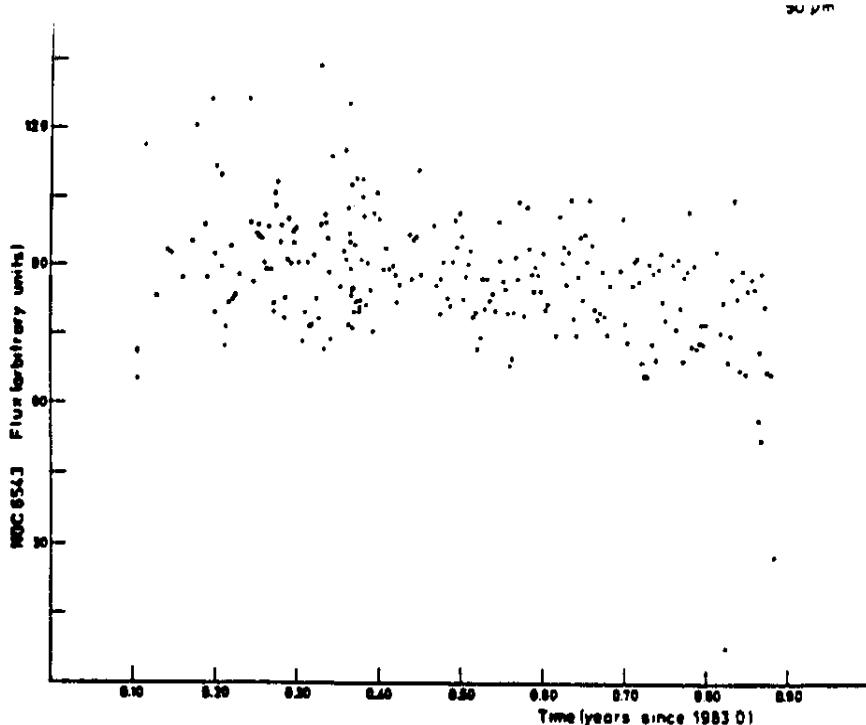


Fig. 8.2. Photometric stability and repeatability, from external calibrations.

Responses to the transfer photometric reference source, NGC 6543, are plotted versus time. In both bands the responsitivity dropped by 30 % per year, an effect that was accounted for in the final calibration procedure. The internal accuracy of these observations is about 15 % r.m.s.

Before  $t = 0.30$  years the scatter in the flash intensity is rather large because the flashes were observed on the source. Therefore we fitted a straight line to the flash intensities beyond  $t = 0.30$ , and found a r.m.s. deviation of about 25 % for both bands. This value can be interpreted as an estimate of the repeatability of CPC observations of low signal-to-noise.

There is a barely significant decrease of the response of CPC to the flashes in the course of the mission, confirming the decrease found on celestial sources (see below).

### 8.1.2. NGC 6543

A similar plot as Fig. 8.1 is shown in Fig. 8.2 using NGC 6543 as a constant source. (The NGC 6543 observations used have not been fully processed: the correction for long-term responsivity variation has not been applied.) A histogram of the flux values indicates that the distribution of flux values resembles a gaussian, and there are about 20 of the 247 flux values that lie very far from the average value. Ignoring those 20 values we have derived one sigma values of 12 % and 17 % at 50 and 100  $\mu\text{m}$  respectively. These values can be interpreted as the repeatability of CPC for sources like NGC 6543:

- lying far away from the galactic plane, and
- not observed just after a passage over the South Atlantic Anomaly.

There clearly is a decrease of long-term responsivity in the course of the mission. Because of the large scatter precise numbers cannot be derived. For the data reduction (see section 6.6) we have used a linear decrease, arbitrarily normalised to 1 at epoch 1983.0, derived from a best fit in Fig. 8.2.

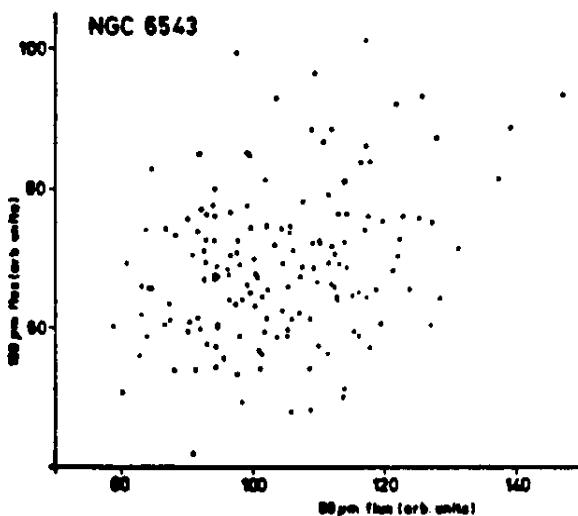


Fig. 8.3. Repeatability of the ratio of the 50 and 100  $\mu\text{m}$  responses to NGC 6543.

Clearly there is very little correlation between the responsivity variations observed in the two channels.

The fairly bad reproducibility derived above is quite probably due to the responsivity variation effect. In figure 8.3 the 100  $\mu\text{m}$  flux is plotted versus the 50  $\mu\text{m}$  flux of each individual NGC 6543 observation. The scatter is considerable indicating that the responsivity variations of the 50 and 100  $\mu\text{m}$  bands of a simultaneous observation are not correlated.

## 8.2. Linearity and absolute calibration

To determine the linearity and absolute calibration of the CPC a number of observations on point sources were compared with the results of IRAS survey observations.

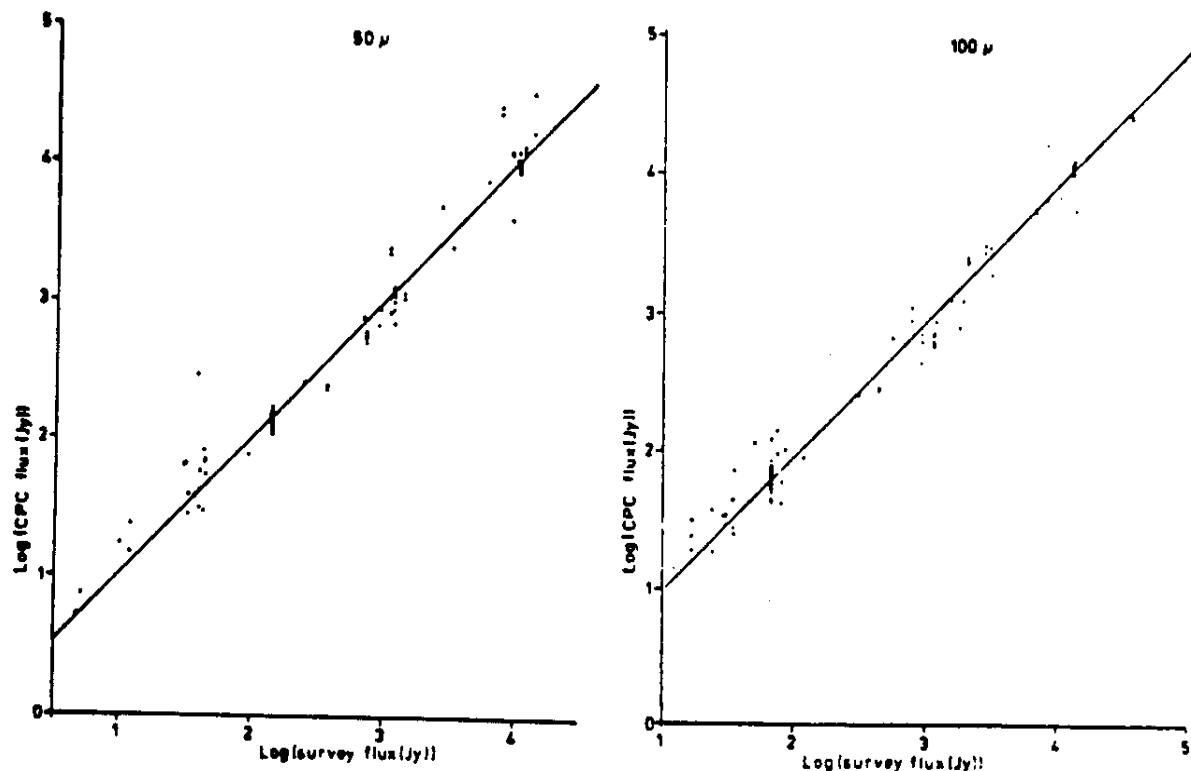


Fig. 8.4. Absolute calibration of the CPC.

For 50 point sources this figure shows the correlation between flux densities from CPC observations and from the IRAS Point Source Catalogue. Apart from a scatter of about 50%, the data can be fitted with a linear relation, indicated in the figure. This relation defines the calibration of the CPC results.

About 50 sources were selected from the CPC maps as being completely mapped by the CPC observations, i.e. FWHM less than about 2 arcmin at both 50 and 100  $\mu\text{m}$ . The point source flux density as observed by CPC was determined in instrumental units, by integrating the surface brightness over the whole map with subtraction of the background level. The background surface brightness was taken as the median of the distribution of brightness values in the map. For the selected type of sources, the distribution of brightness values is dominated by the background pixels, and the median value is accurate as background level to within 3 percent. The results were plotted against the IRAS survey point source catalog fluxes (see Fig. 8.4). The CPC 50  $\mu\text{m}$  flux density was compared with the survey 60  $\mu\text{m}$  flux density, and the CPC 100  $\mu\text{m}$  with the survey 100  $\mu\text{m}$ . No color corrections were made to allow for deviations from a flat spectrum.

From these plots three conclusions can be drawn.

1. The CPC photometers are linear as compared with the survey instrument over a dynamic range of 4 decades.
2. The calibration of the instrumental units can be derived by determining the best fitting straight line of slope 1 in the plots of fig. 8.4. A correction factor of 50/60 was used to convert flux densities at 60  $\mu\text{m}$  to 50  $\mu\text{m}$ , i.e. sources with a flat spectrum in  $\nu F_\nu$  were assumed in this calibration. The result is given in table 6.1.
3. For individual objects, a CPC-based point source flux density can deviate by 50 percent, even though the CPC maps for repeated observations of a single source reproduce the surface brightness to about 15 percent (see section 8.1).

The disappointing reliability of the CPC surface brightness calibration for single observations may partly be explained by the fact that we did not use any color corrections in the comparison, partly by systematic effects in the different methods of flux determination: for the CPC we integrated surface brightness over the source area, whereas the catalog result is based on a template fit.

We think however that the major part must be ascribed to responsivity variations. We recommend that the flux calibration of individual CPC observations be compared with IRAS survey data results. This can be done by determining the point source flux density as outlined above, and comparing with the point source catalog flux density. As an alternative, the surface brightness in the CPC map may be compared with the extended emission products of the IRAS survey.

### 8.3. NGC 6543 as reference source

The planetary nebula NGC 6543 was chosen as reference source for the IRAS mission, as it appears to be a sufficiently strong non-variable IR source. Daily measurements of this object allow determination of the repeatability of observations and of long-term variation in the responsivity of the CPC. The response on NGC 6543 was also used as a check on the absolute calibration.

Several properties of NGC 6543 may have influence on the final calibration. Situated at galactic latitude 29°1, the risk of confusion with galactic sources is low. Inspection of Skyflux maps of the region around NGC 6543 confirm that NGC 6543 is an isolated IR source.

Optically, NGC 6543 is a bright compact HII region of approximately 10 arcsec in radius, surrounded by a weak halo of 190 arcsec radius (Millikan, 1974). The IR emission distribution as observed by CPC in the 50  $\mu\text{m}$  band is shown in figure 8.5. With the effective solid CPC beam derived in section 5.3 the nebula appears unresolved. Moseley (1980) has attempted to determine the size of NGC 6543 in 37  $\mu\text{m}$  continuum radiation; he found little flux outside his beam of 20 arcsec diameter. There is no evidence in single CPC images that a halo is present at 50 and 100  $\mu\text{m}$ .

Planetary nebulae do not only emit IR continuum radiation, but also line radiation in forbidden lines. Known planetary nebula emission lines in the survey and CPC passbands are [OIII] at 52  $\mu\text{m}$ , [NIII] at 57  $\mu\text{m}$  and [OIII] at

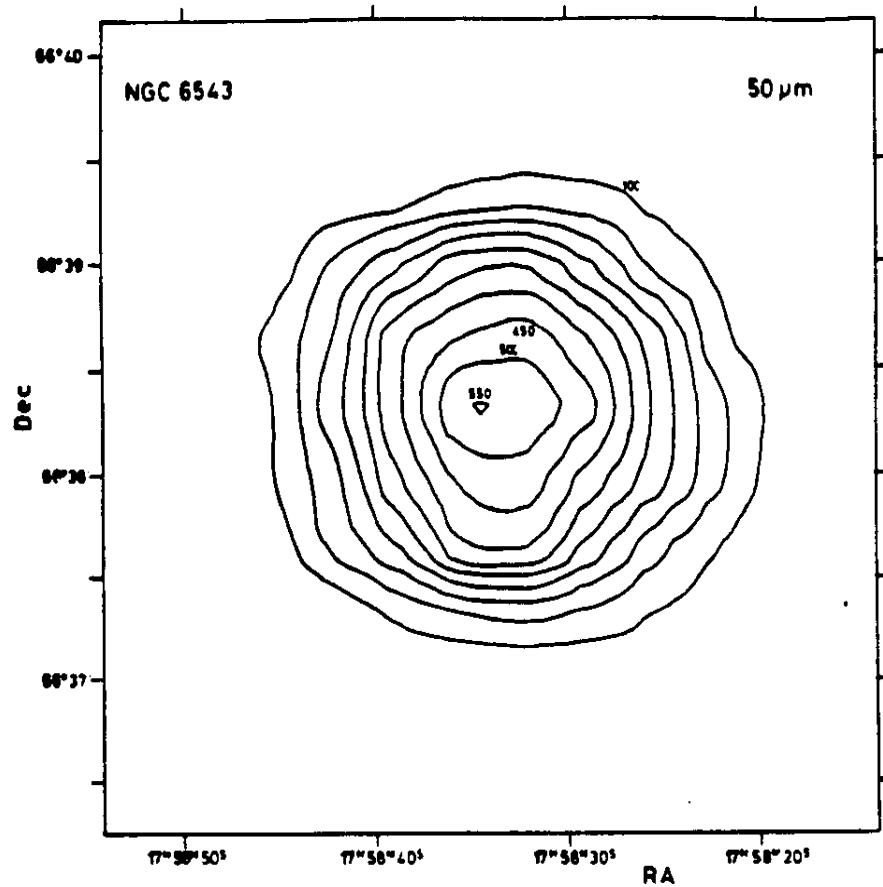
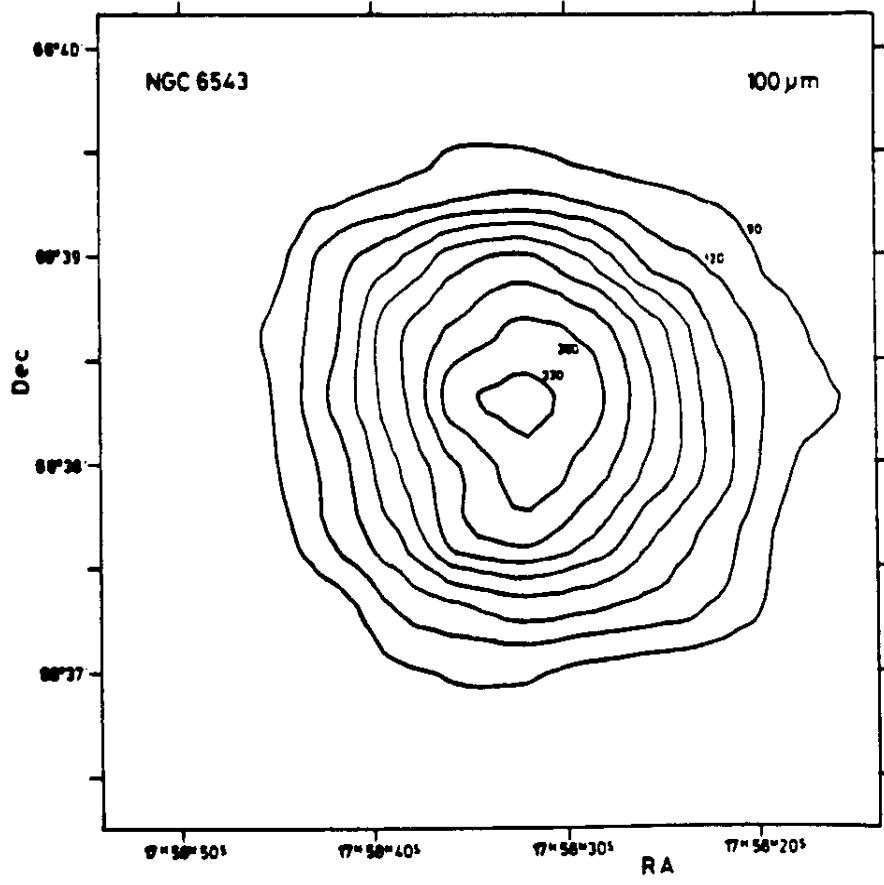


Fig. 8.5. Contour plots of NGC 6543 at 50 and 100  $\mu\text{m}$ .

An arbitrary observation of this planetary is shown. The brightness unit is 1 MJy/sr. An individual observation does not show any extended structure.



88  $\mu\text{m}$ .

The 52  $\mu\text{m}$  and 57  $\mu\text{m}$  lines appear in both the CPC 50  $\mu\text{m}$  band and the survey 60  $\mu\text{m}$  band (see figure 4.1). Watson et al. (1981) measured the 52  $\mu\text{m}$  line intensity in NGC 6543 as  $2.6 \times 10^{-13} \text{ W m}^{-2}$ . An upper limit on the intensity of the 57  $\mu\text{m}$  line can be derived by assuming (i) all N is ionized into  $\text{N}^+$ , and using known parameters such as electron density and temperature (Pottasch et al., 1984). The 57  $\mu\text{m}$  line intensity is then at most  $8.5 \times 10^{-13} \text{ W m}^{-2}$ . The in-band flux at 60  $\mu\text{m}$  was found to be  $3.4 \times 10^{-12} \text{ W m}^{-2}$  (IRASES 1985), which is considerably larger than the estimated flux in the lines. Since both lines are located well inside both the 60  $\mu\text{m}$  survey and 50  $\mu\text{m}$  CPC bands, their influence on the calibration of the 50  $\mu\text{m}$  CPC measurements is negligible.

The strength of the 88  $\mu\text{m}$  line can be estimated from the 52  $\mu\text{m}$  line intensity, the electron density and temperature in the nebula. In this way an intensity of  $5 \times 10^{-14} \text{ W m}^{-2}$  is derived. As the in-band flux in the 100  $\mu\text{m}$  survey band is  $7.6 \times 10^{-13} \text{ W m}^{-2}$ , and the line again appears both in the CPC and survey 100  $\mu\text{m}$  bands, the influence on the comparison of CPC and survey fluxes of NGC 6543 is negligible.

We assume, upon the arguments presented above, that the contributions of line radiation are about equal in the survey and CPC bands. We also assume that the underlying continuum can be represented closely enough by a 135 K blackbody curve for computing color corrections. The survey flux densities can then be converted to the following flux densities at the CPC wavelengths:

$$\begin{aligned} F_{50 \mu\text{m}} &= 140 \text{ Jy}, \\ F_{100 \mu\text{m}} &= 67 \text{ Jy}. \end{aligned}$$

In conclusion, the measured fluxes within the broad photometric bands of the CPC and survey instrument are mainly due to thermal continuum radiation from heated dust particles. It was therefore justified to use NGC 6543 to monitor the calibration, repeatability, and stability of both instruments.

References.

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## A.1. Description of CPC Deglitch Routines.

The deglitch routines have two main functions: the demodulation of the raw data and the removal of the frequently occurring glitches. Both functions will be described in some detail below.

Capitalized words refer to procedures or functions of the deglitch software.

### A.1.1. Demodulation

The photometric data as they came from the satellite were modulated with a frequency  $f_m = 15.062$  Hz. They were sampled 64 times per second ( $f_s = 64$  Hz). In a trade-off between high time resolution versus computing time and unwanted beat frequencies, we settled on a demodulation of 8 data-points in one turn, bringing the data frequency down to 8 Hz. For the  $k$ -th point we can write:

$$x_k = b + a \cos(\phi + k \Delta\phi) \quad (1)$$

where  $b$  is the dc-value,  $a$  is the amplitude and  $\phi$  is the phase of the modulated signal.  $\Delta\phi$  is  $2\pi f / f_m$ .

Equation (1) can be written as a linear equation in  $b$ ,  $a \cos\phi$  and  $a \sin\phi$ :

$$x_k = b + a \cos\phi \cos(k \Delta\phi) - a \sin\phi \sin(k \Delta\phi) \quad (2)$$

From this set of 8 equations the amplitude,  $a$ , can easily be solved.

FILMAT sets the constants  $\cos(k \Delta\phi)$  and  $\sin(k \Delta\phi)$  and fills the inverted matrix; DEMOD performs the demodulation of 8 raw data points, yielding one point for 1/8 sec.

### A.1.2. Deglitcher

#### A.1.2.1. Definition of a Glitch

Glitches come in two kinds: random glitches and photon induced glitches. Both kinds have positive and negative representatives, of which the positive ones are in the majority.

The random glitches are presumably caused by particle hits on the detectors. They occur independent of what the detector is looking at. The cause of the photon induced glitches is less clear. They only occur when a certain amount of flux is shining on the detector. By lack of a more apt name they are called photon induced glitches. Although these two kinds clearly occur, there is a large overlap area where glitches cannot be ascribed to either kind.

In general a glitch is characterized by a fast rise time and an exponential decay. Mostly the top is reached within 0.1 second. Sometimes strange starting effects occur e.g. a deep negative trough just before a positive glitch which are caused by the dc restorer. Negative glitches do not have these strange starting effects. After reaching the top the glitch decays within 1 second to half the top value; it is not possible to define one characteristic decay time. The random glitches seem to be faster than the photon induced ones. Some characteristic glitches are shown in figures A.2 and A.3

#### A.1.2.2. Removal of a Glitch

The routines for removal are operating on a window of 4 seconds; Fig. A.1 defines the terms: backend, frontend and point.

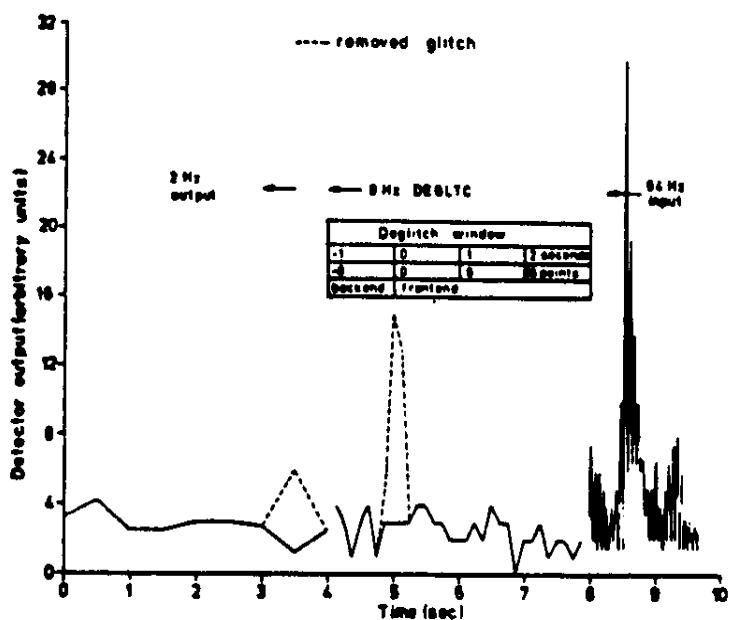


Fig. A.1. Removal of a glitch

The removal method uses a window of 4 seconds. The terms "backend", "frontend" and "point" are explained.

At the start the window is filled (FILWINDOW). The data in the backend are used to determine the background level and its noise. A linear equation is fitted to these points which are weighted with a geometric decay. For computational reasons this particular weighting scheme was chosen: in a scheme where all points on a certain stretch of the backend have equal weight, computational errors tend to accumulate just enough to be noticeable at the end of one measurement (about 400 seconds). The geometric decay avoids this nuisance.

The weight is  $\tau^{|i|}$ , where  $i$  is counted from zero and  $\tau$  is chosen to be 0.8. Effectively the fit is made to only 5 points but a  $\tau$  equal to 0.9 (10 points effectively) yields a fit that reacts too slow on a fast crossing of a source. The noise is determined from the sum of the squared deviations. A minimum value on the noise is necessary as the subtracting mechanism in the deglitcher diminishes the number of degrees of freedom in the noise. The value of 0.0001 Volts is taken as it is the smallest value the raw data could at-

tain.

From here on the background to a point is an extrapolation of the linear fit to that point. The noise is supposed to be constant over this extrapolated region.

As the actual filtering of glitches starts at point zero, the first second of every measurement or after a gap in the datastream, is not deglitched. In all other situations the background and noise are determined from deglitched data of the backend.

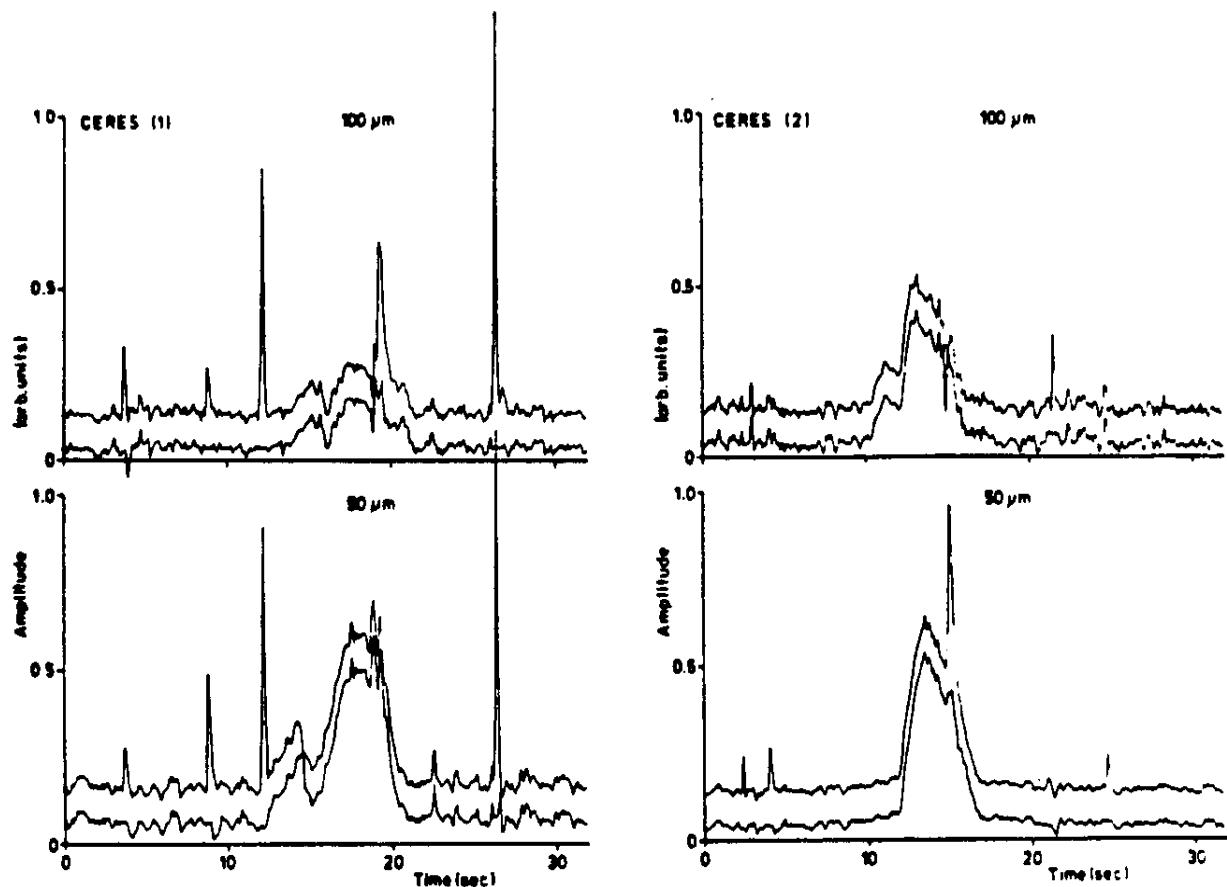


Fig. A.2. Examples of CPC data before and after deglitching.

The figures show 8 Hz data, original (top trace, shifted upward) and deglitched.

- Figure Ceres (1).

Some random glitches can be seen, often correlated between both channels. Ceres is visible between 12 and 20 sec.

- Figure Ceres (2).

Some random glitches are present. A nice example of a strong negative glitch occurs at 100  $\mu$ m at 15 sec; it is correlated with a very strong positive glitch at 50  $\mu$ m.

In order to be recognised a glitch as defined above has to fulfill 4 conditions. (Note that for negative glitches all signs have to be reversed.)

1. At point 2 the strength of the glitch i.e. the signal minus the back-

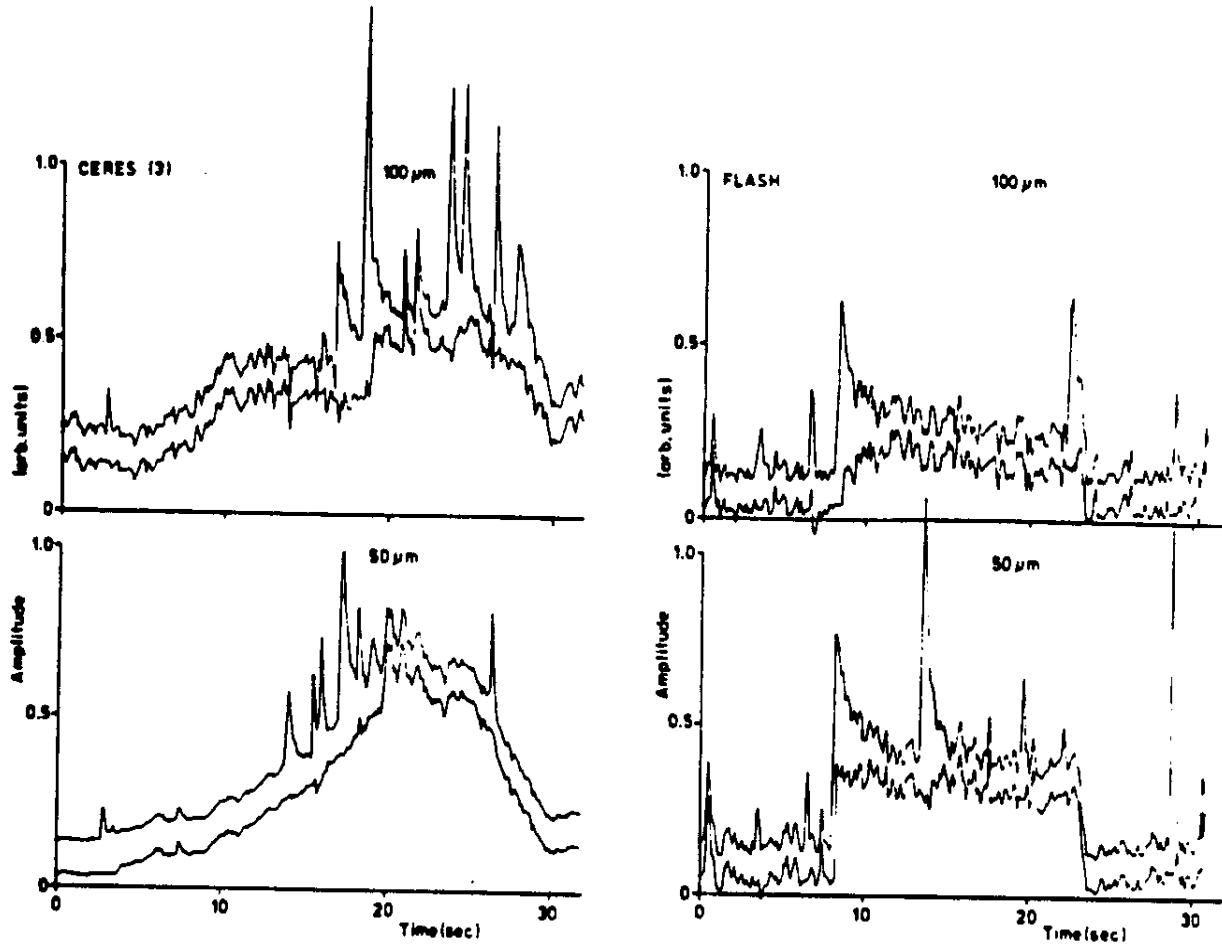


Fig. A.3. Examples of CPC data before and after deglitching.

The figures show 8 Hz data, original (top trace, shifted upward) and deglitched.

- Figure Ceres (3).

Conspicuous photon-induced glitches appear on the leading wing of Ceres. They are somewhat broader than the random glitches. Note that at 50  $\mu\text{m}$  at 20 sec a complicated 'double' glitch occurs which the deglitcher could not handle. At 26 sec a positive glitch shows a negative start (100  $\mu\text{m}$ ).

- Figure Flash.

At the beginning of a flash usually a photon-induced glitch is seen. This kind of glitch can be removed by the feature described in Annex.1 (condition 4).

ground, has to be greater than 7 times the noise. Point 2 was chosen to step over the strange starting behavior of some glitches (FORNEXTTIME). Seven as a glitch recognition constant is a compromise between cutting in the noise (at 5) and leaving conspicuous glitches untouched (at 10).

2. When earlier in time the subtraction of a glitch already occurred at point 2, we don't want to subtract other glitches which could be artefacts of our own manipulation. More stringent rules have to be applied now. The candidate glitch has to be greater than 4 times the difference between the original and the manipulated signal which allows a glitch in the tail of a previous one to be subtracted, or it has to be greater than 14 times the noise; it has to be really huge. The values of both constants have a certain amount of arbitrariness (CONFUSION).
3. A candidate glitch has to have a top within a certain (time)interval i.e.

a point which is higher than the previous one and the next one. The interval is confined to the points 2 or 3 which limits the rising time to 0.25 seconds (NOTOP).

4. After having a top a candidate has to decay to half of its strength within a certain (time)interval (less than 6 points). When no decay within this interval is found it is tried again with a new glitch strength equal to half of the old one. This is repeated until the new strength is less than 7 times the noise, in accordance with condition 1 or, of course a decay is found. This last feature gives a handle on e.g. glitches at the beginning of a flash. See figure A.3.  
Here also the decaytime from the top is calculated. The exact time of half signal strength is linearly interpolated between the two encompassing points. The decay time equals half signal time minus top time (in seconds). For very short glitches with a decay within one point, the decaytime is determined by fitting an exponential to the first point after the top (NODECAYTIME).

If a candidate glitch fulfills all 4 conditions it is supposed to be a genuine one and it can be subtracted. From the begin to the top the signal is set to the background. From the top to 6 times the decaytime an exponential is subtracted with strength and decaytime as determined (FILTER).

After a search for a glitch, succesful or not, the window is shifted one point (ROLLOVER), the background is determined anew (NIVEAU) and the conditions for a glitch are applied to the next zeropoint. After 8 of those shifts the backend of the window is full of new points. Of both the original and the deglitched signal half-second means are taken which are returned to the main program with the corresponding satcal and a quality measure. The quality measure is defined as the number of points which were left unchanged by the deglitcher; so it runs from 0 to 4. (TAKEMEAN)

When a gap in the data stream occurs the window is emptied first via FILTER, ROLLOVER and TAKEMEAN, after which the window can be filled again with FILWINDOW. The end of the data stream is treated as a gap with the exception that the window is not filled again. The steering between normal and 'gap' performance is done by DGLSTEER.

## A.2. Discussion of some sample maps

### A.2.3. NGC 6543

This is one of the many observations of the planetary nebula, NGC 6543, our photometric reference source. It is a source of reasonable strength and it is indistinguishable from a point source for the CPC instrument.

The noise is below 5 % and 15 % for the 50 and 100  $\mu$  channel respectively. The background lies at 20 MJy/sr for both channels.

Some of the responsivity variation phenomena appear. From the start of the observation (indicated with an arrow, pointing in the in-scan direction) to the end the background increases by about 30 %. The variation is taken out by the gain correction program. The difference between the increasing and the flat background is evident by comparing the 'raw' and the 'clean' map.

Another responsivity variation effect is the distortion in the in-scan direction of the lower contour lines, best seen in the 50  $\mu$  'clean' map. In general features parallel to the in-scan direction should be treated with caution: they could be spurious. In this example map the effect is not very strong; it disappears at the 10 % level and at 100  $\mu$  it is not seen at all. For sources fainter than NGC 6543 the effect will be of small or no importance.

### A.2.4. NGC 3610

The target of the observation was a galaxy, NGC 3610, but obviously it is not detected.

All 'structure' in the map has a size smaller than or equal to the beam-size. This 'structure' must be noise. The dynamic range is a factor 4 to 6 and the mean flux level is about 13 MJy/sr for both channels. This is approximately the lowest CPC background found. The noise in the map is accordingly (~ 4 MJy/sr per pixel). This noise is dominated by a large number of small to very small glitches which could not be detected by the deglitch program. The larger glitches, present in abundance in the 'raw' map, have been cut out quite satisfactory.

Around the edges of the map the noise is somewhat larger than in the interior. This is due to the fact that at the edges sometimes only one point contributes to the pixel, while in the interior a pixel is always the mean of several points measured.

#### A.2.5. Ceres

Ceres is an asteroid, and a true point source. It is somewhat more intense than NGC 6543 and all effects described above can also be seen.

Glitches are large and abundant as the observation was done near the South Atlantic Anomaly. The deglitcher is able to take these out.

The gain is increasing with a factor 1.5 and 2.5 for 50  $\mu$  and 100  $\mu$  respectively. Correcting for it was no problem due to the fact that Ceres is a simple point source on a (presumably) flat background of 50 and 20 MJy/sr.

#### A.2.6. MRSI 269-01/2

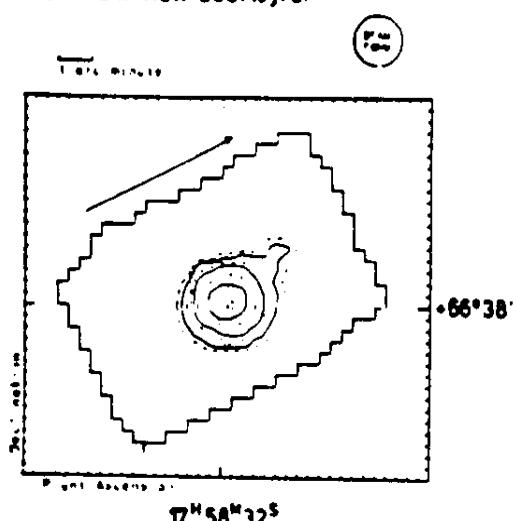
This is a molecular cloud region. The true shape of the cloud is severely distorted by the responsivity variation effect (section 5.1). At the high flux levels of this source glitches are of no importance anymore; they drown in the source flux.

The source is clearly extended, but the true size and shape is difficult to establish from this CPC map. The routine correcting for the long-term increase of the background fails, because the definition of background is moot. The program calculates gain increases of 3 and 5 on 'mean background levels' of 300 and 1100 MJy/sr for 50 and 100  $\mu$ m respectively.

We decided to exclude maps from the CPC atlas where the gain correction did not meet certain stringent conditions. This particular image is an example of an excluded one.

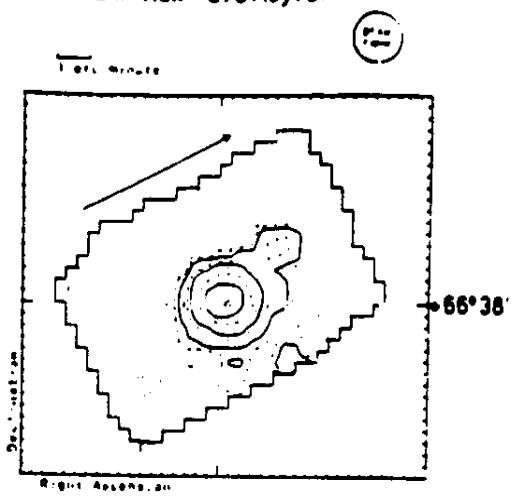
### NGC6543 IRAS CPC CLEAN IMAGE

band 50 micron  
minimum flux 11 MJy/sr  
maximum flux 560 MJy/sr



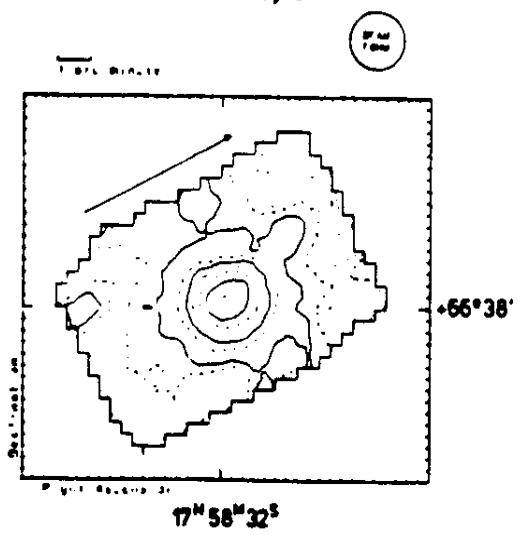
### NGC6543 IRAS CPC RAW IMAGE

band 50 micron  
minimum flux 10 MJy/sr  
maximum flux 570 MJy/sr



### NGC6543 IRAS CPC CLEAN IMAGE

band 100 micron  
minimum flux 12 MJy/sr  
maximum flux 290 MJy/sr



### NGC6543 IRAS CPC RAW IMAGE

band 100 micron  
minimum flux 13 MJy/sr  
maximum flux 290 MJy/sr

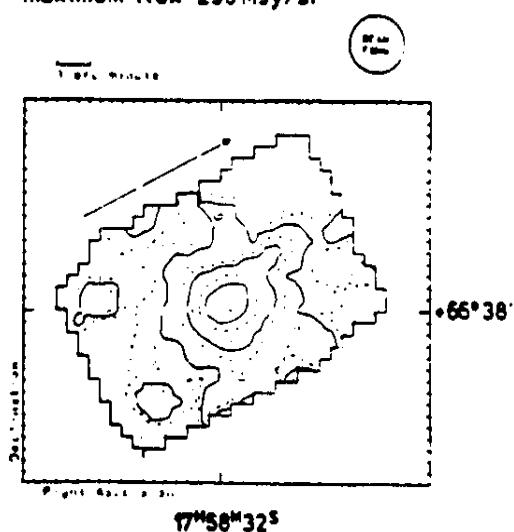
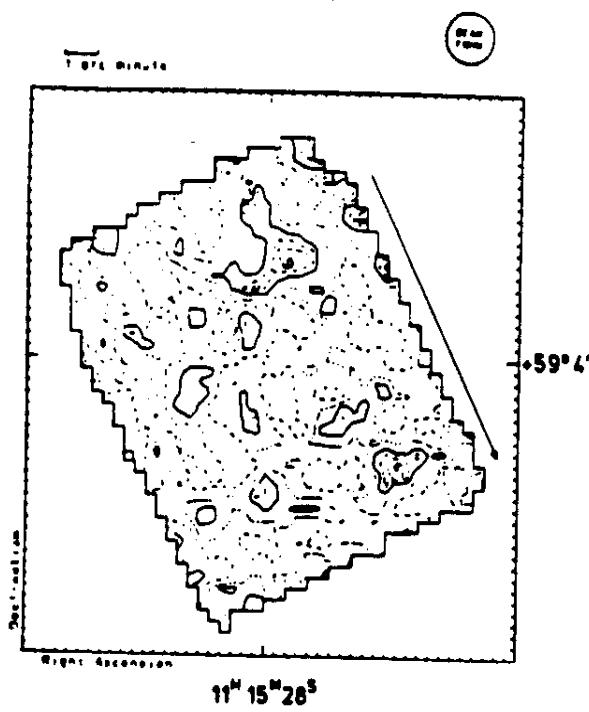


Fig. A.4 Example of a CPC map. See text for a discussion.

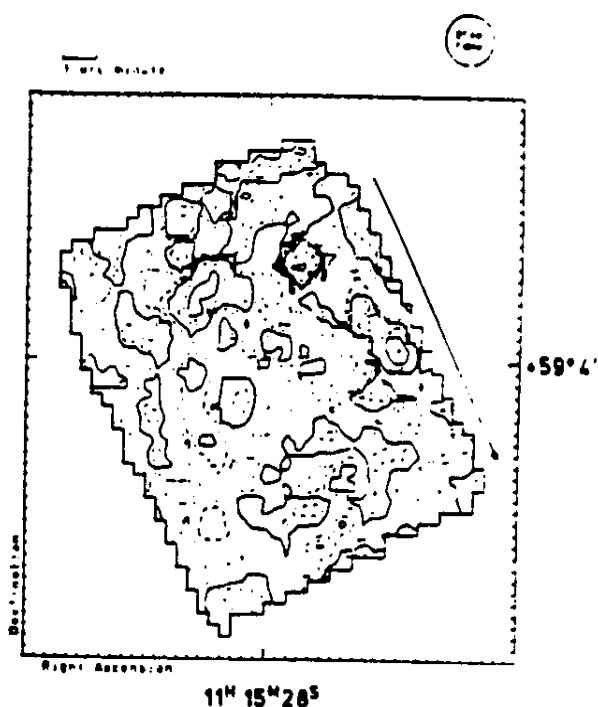
NGC3610 IRAS CPC CLEAN IMAGE

band 50 micron  
minimum flux 8 MJy/sr  
maximum flux 62 MJy/sr



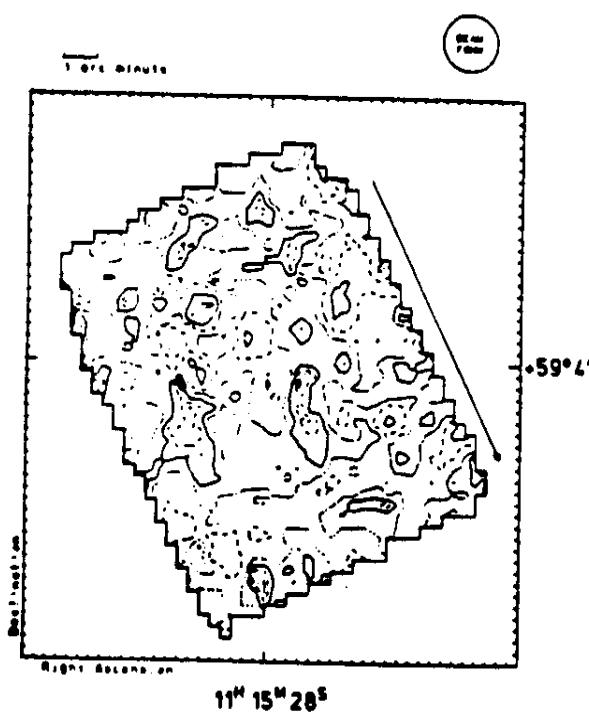
NGC3610 IRAS CPC RAW IMAGE

band 50 micron  
minimum flux 8 MJy/sr  
maximum flux 166 MJy/sr



NGC3610 IRAS CPC CLEAN IMAGE

band 100 micron  
minimum flux 10 MJy/sr  
maximum flux 58 MJy/sr



NGC3610 IRAS CPC RAW IMAGE

band 100 micron  
minimum flux 10 MJy/sr  
maximum flux 130 MJy/sr

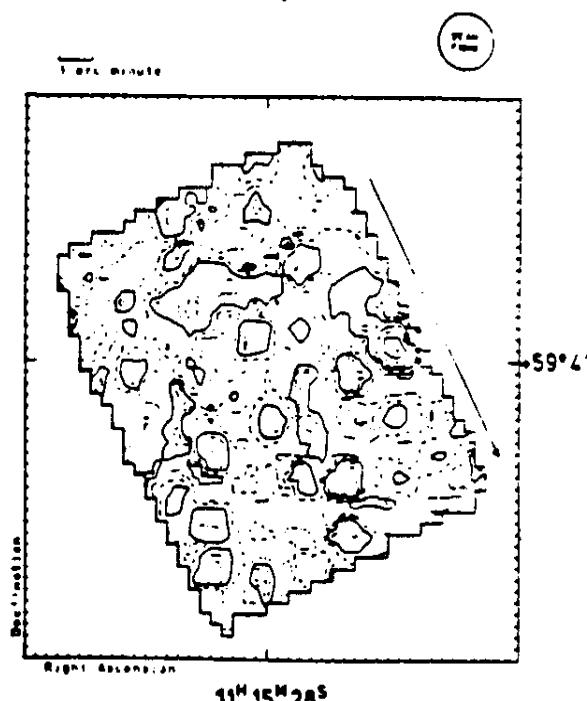
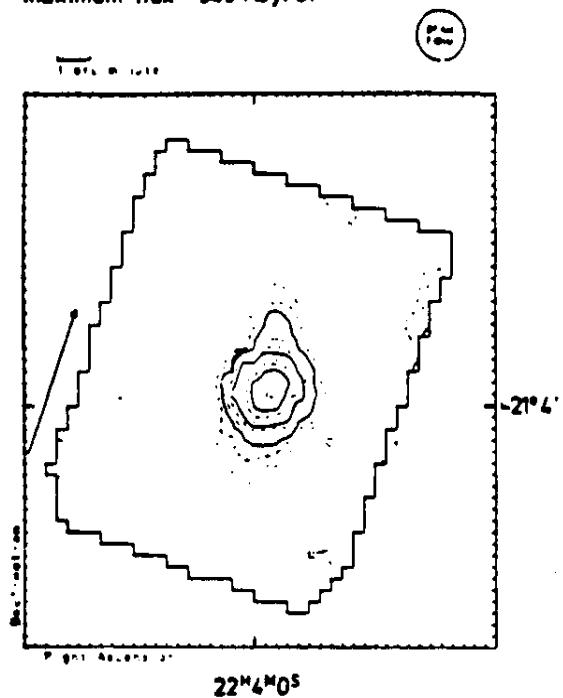
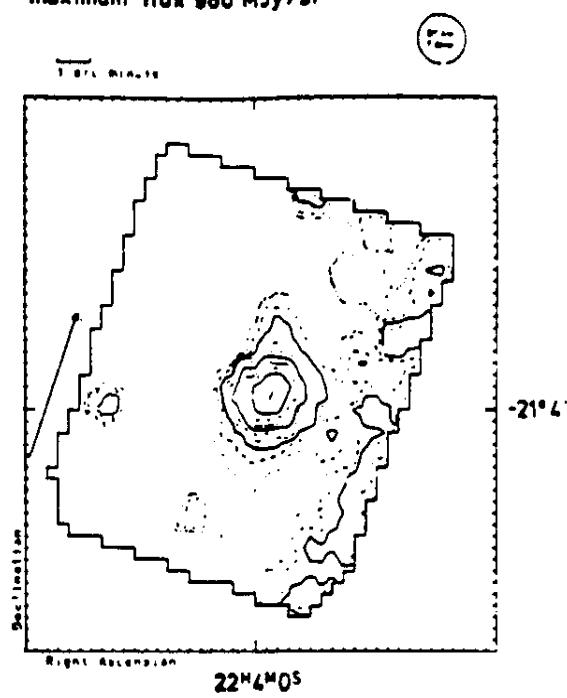


Fig. A.5 Example of a CPC map. See text for a discussion.

band 50 micron  
minimum flux 23 MJy/sr  
maximum flux 960 MJy/sr

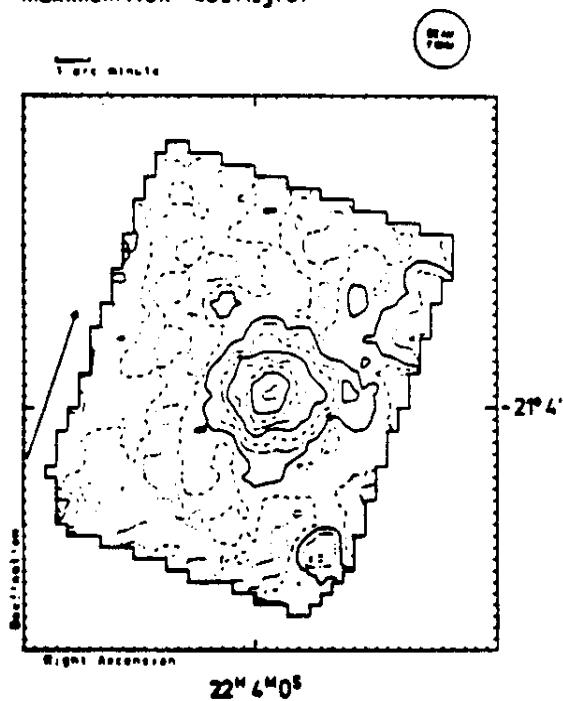


band 50 micron  
minimum flux 26 MJy/sr  
maximum flux 960 MJy/sr



### CERES IRAS CPC CLEAN IMAGE

band 100 micron  
minimum flux 8 MJy/sr  
maximum flux 450 MJy/sr



### CERES IRAS CPC RAW IMAGE

band 100 micron  
minimum flux 8 MJy/sr  
maximum flux 450 MJy/sr

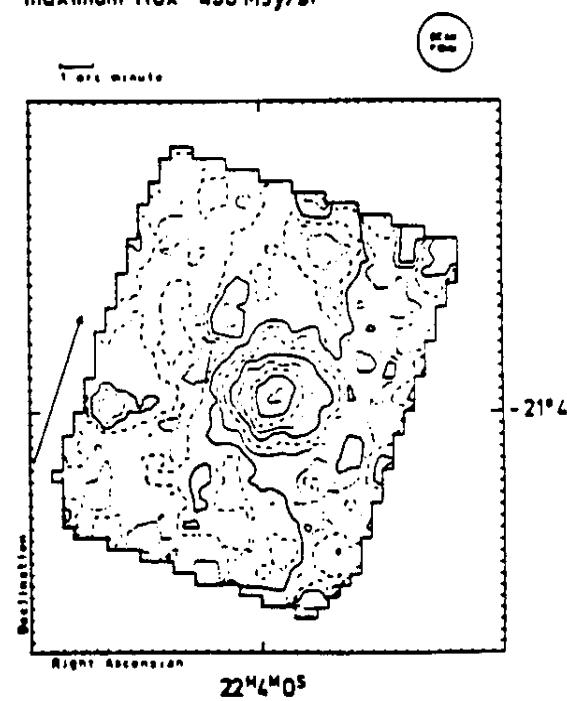
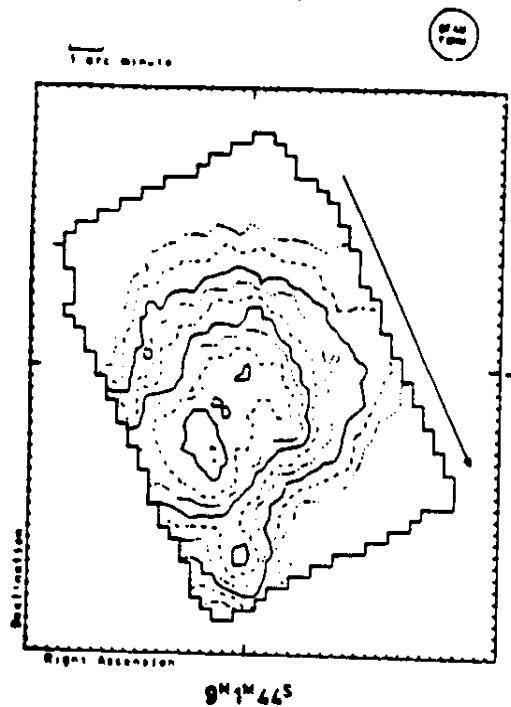
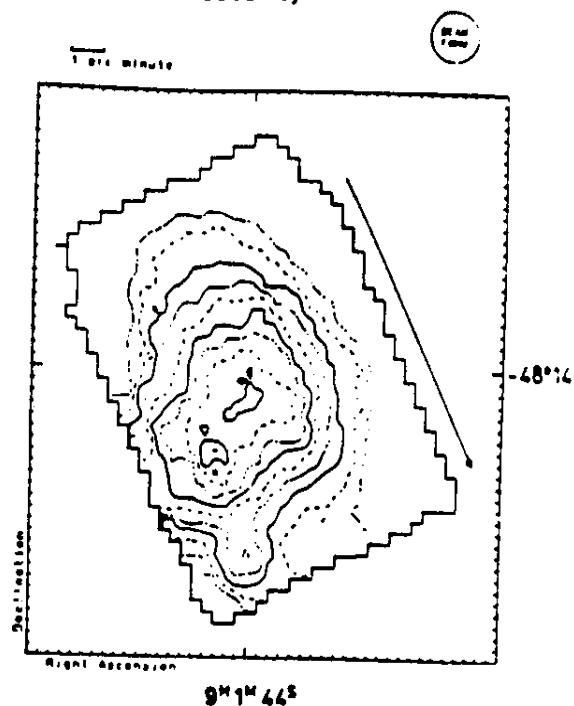


Fig. A.6 Example of a CPC map. See text for a discussion.

band 50 micron  
minimum flux 280 MJy/sr  
maximum flux 5300 MJy/sr

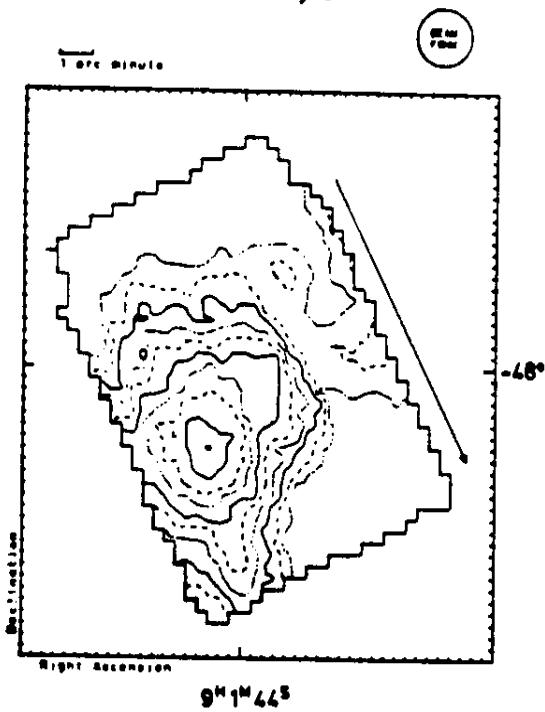


band 50 micron  
minimum flux 120 MJy/sr  
maximum flux 5600 MJy/sr



### MRS 269-01/2 IRAS CPC CLEAN IMAGE    MRS 269-01/2 IRAS CPC RAW IMAGE

band 100 micron  
minimum flux 1200 MJy/sr  
maximum flux 12000 MJy/sr



band 100 micron  
minimum flux 210 MJy/sr  
maximum flux 1200 MJy/sr

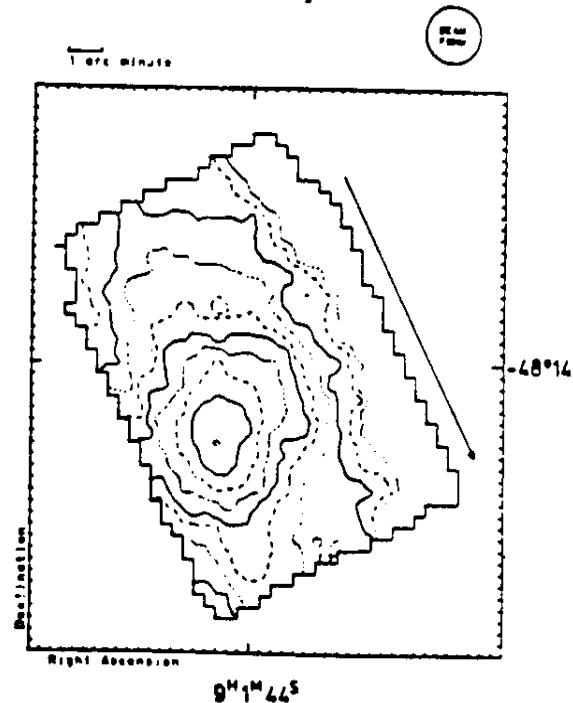


Fig. A.7 Example of a CPC map. See text for a discussion.

### A.3. Tape Format

The CPC observations are distributed on magnetic tape in FITS format, with a corresponding tape density of 1600 bpi and blocksize of 2880 bytes. The FITS format is described in Wells (1980). There are two consecutive FITS files on the tape for each observation, one giving the "clean" and the other the "raw" images (see section 3 and 6.6). In each file two maps (at 50 and 100  $\mu$ m) are stored in a three dimensional array, where the first axis denotes the right ascension and the second the declination. The third dimension gives the wavelength.

There are 1508 CPC observations distributed on 3 output tapes. For identification purposes, the actual tape in FITS format is preceded by a tape label group, 2 80-byte tape blocks of ASCII characters and a tape mark, written in the format of an ANSI label group. Note that this is at variance with both the FITS standard, which does not specify labelling, and with the ANSI standard, which uses tapemarks only to separate data and label groups, and prescribes trailer label groups as well.

Table A.1. Distributed tapes

Tape label	number of observations	RA range (hours)
LPCFT1	469	00 - 07
CPCFT2	624	08 - 15
CPCFT3	395	16 - 23

A list of all observations, sorted on RA/DEC is appended after the FITS images on the tape CPCFT3.

#### A.3.7. Header of list of observations

The list of the distributed observations, added after the FITS images on the last tape CPCFT3, is written in the FITS table extension format (Harten et al., 1984) The format used is the same as that of column 1-5 of annex 4.

#### A.4. List of observations

The columns indicate :

1. Conventional astronomical object name (if known).
2. Julian epoch of observation - 1983.0.
3. Map centre Right Ascension 1950.0.  
The list is sorted on Right Ascension.
4. Map centre Declination 1950.0.
5. Observation type used.

The abbreviations used for the observation types differ slightly from the macro names used in Table 2.1, e.g. CPCF9A = 9\*9FF, CPC09A = 9\*9F.

6. Declination error warning.  
A "1" in the sixth column indicates that the decoding of the declination sent up to the satellite might be in error.
7. Deleted observation flag.  
"BADGAIN" in column 7 means that the measurement could not satisfactorily be corrected for the sensitivity variation phenomenon discussed in section 5.1. Such observations have been deleted from the processing chain, and can consequently not been found on the CPC tapes. In some cases it might be possible with the help of Groningen experts to interpret the data of such measurements. Interested astronomers should contact P.R. Wesselius.

### A.3.8. Header of FITS image

To prevent a proliferation of keywords we give qualitative information in comments. As an example, and to show the keywords we have used, an arbitrary FITS header is shown below.

```
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214)
BITPIX = 16 / PIXEL VALUES: 2-BYTE TWOS-COMPLEMENT INTEGERS
NAXIS = 3 / NUMBER OF AXES IN THE DATA ARRAY
NAXIS1 = 47 / NUMBER OF PIXELS/ROW (RA) (COLUMNS)
NAXIS2 = 51 / NUMBER OF ROWS (DEC)
NAXIS3 = 2 / NUMBER OF WAVELENGTHS (LAMBDA)
CTYPE1 = 'RA'      ' / COORDINATE TRANSFORMATIONS:
CRVAL1 = 1.33967E+02 / X OF PIXEL = (COLUMN - CRPIX1)*CDELT1
CRPIX1 = 2.40000E+01 / Y OF PIXEL = (ROW - CRPIX2)*CDELT2
CDELT1 = -5.55556E-03 /
CTYPE2 = 'DEC'     ' / TRANSFORMATIONS BETWEEN (X,Y) AND (RA,DEC):
CRVAL2 = -4.24833E+01 / APPROXIMATE (FAR FROM THE CELESTIAL POLES):
CRPIX2 = 2.90000E+01 / X = (CRVAL1 - RA)*COS(CRVAL2)
CDELT2 = 5.55556E-03 / Y = DEC - CRVAL2
CTYPE3 = 'LAMBDA'   ' / EXACT:
CRPIX3 = 1.00000E+00 / X = SIN(CRVAL1 - RA)*COS(DEC)
CRVAL3 = 5.00000E-05 / Y = (SIN(DEC)*COS(CRVAL2)) -
CDELT3 = 5.00000E-05 / (COS(DEC)*SIN(CRVAL2)*COS(RA-CRVAL1))
BSCALE = 2.58334E-02 / DATA SCALE FACTOR (REAL-TAPE*BSCALE+BZERO)
BZERO = 9.26282E+02 / DATA OFFSET VALUE
BUNIT = 'MJY / SR' / BRIGHTNESS UNITS
BLANK = -32767 / TAPE PIXEL VALUE ASSIGNED TO UNDEFINED VALUE
DATE-OBS= '24/06/83' / DATE OF OBSERVATION (JE 1983.481044)
TIME-OBS= '22:48:49' / TIME OF OBSERVATION
INSTRUME= 'IRAS-CPC' / INSTRUMENT USED IN OBSERVATION
ORIGIN = 'ROG-GRON' / NAME OF INSTITUTE THAT PRODUCED THIS FILE
OBJECT = 'VHE 27B'    ' / NAME OF THE OBSERVED OBJECT
COMMENT IRAS CPC CLEAN IMAGE
COMMENT NOSSEBEFORE NOSSEAFTER
COMMENT START OF SCAN AT (COL,ROW)=(22,47) TO (COL,ROW)=(32,39) IN 10 SECONDS.
HISTORY IMTOFTD1 850309 < REGRIDD2 850127 < GAINCRD3 850127 < CPCATTD3 850127
HISTORY < DEGLTCD1 841003
COMMENT THIS TAPE CONTAINS CONFIDENTIAL DATA
COMMENT PUBLICATIONS BEFORE DEC 1985 ARE RESTRICTED TO IRAS PROJECT SCIENTISTS
DATE = '09/03/85'      / CREATION DATE OF THIS FITS TAPE FILE
END
```

#### Remarks:

- When the words 'nosSEbefore' or 'noSSEafter' appear in a COMMENT line, the sighting of a star before or after the rasterscan failed. The attitude reconstruction is not fully reliable.
- The direction and the speed of the scan are indicated in a COMMENT by giving the position of the first sample and the 20th sample. One should not try to reconstruct the details of the raster scan from this information.



119381	03 26.1	*11 08	9*9FF	1	
133303	03 26.1	*31 00	9*9FF	1	
613981	03 26.2	*31 00	9*9F		
616330	03 26.2	*31 00	9*9FF	1	
113982	03 26.3	*30 60	9*9FF	1	
124660	03 26.3	*30 60	9*9FF	1	
611081	03 26.5	*31 17	9*9F		
613398	03 26.5	*31 17	9*9F		
613984	03 26.6	*31 10	9*9F		
616341	03 26.6	*31 10	9*9F		
619000	03 26.6	*31 02	9*9F		
620371	03 26.8	*31 02	9*9F		
590436	03 29.2	-33 88	9*9F		
659217	03 29.2	-33 88	9*9F		
146627	03 29.4	*60 10	3*3SS	1	
147783	03 29.4	*60 10	3*3SS	1	
232930	03 31.0	-75 23	9*9F		
580364	03 31.7	-36 18	9*9F		
587691	03 31.7	-36 18	9*9F		
148086	03 30.3	*32 00	9*9F	1	
582007	03 40.5	-35 19	9*9F		
656002	03 40.5	-35 19	9*9F		
569556	03 40.5	-47 23	9*9F		
571666	03 40.5	-47 23	9*9F		
655142	03 41.9	*67 57	9*9F		
657197	03 41.9	*67 57	9*9F		
IC 342	671222	03 41.9	*67 57	9*9F	
150112	03 42.0	*67 56	9*9FF	1	
153161	03 42.0	*67 56	9*9FF	1	
157773	03 42.0	*67 56	9*9FF	1	
529087	03 42.9	-41 88	9*9F		
MCC 1448	539082	03 42.9	-44 48	9*9F	
MCC 1448	510058	03 42.9	-44 48	9*9FF	
MCC 1448	534179	03 42.9	-44 48	9*9FF	
UCG 2855	641240	03 43.2	+69 59	9*9F	
UCG 2855	643303	03 43.2	+69 59	9*9F	
UCG 2855	783495	03 43.2	+69 59	9*9F	
URG 2855	199136	03 43.3	+70 00	3*3SS	
UCG 2855	203339	03 43.3	+70 00	3*3SS	
166857	03 55.0	+66 59	9*9FF	1	
190001	03 55.0	+66 59	9*9FF	1	
179942	04 15.0	+41 54	9*9F	1	
182686	04 15.0	+41 54	9*9F	1	
450925	04 17.0	-62 54	9*9F		
463036	04 17.0	-62 54	9*9F		
MCC 1566	528106	04 18.9	-55 03	3*3SS	
MCC 1566	528067	04 18.9	-55 03	3*3SS	
MCC 1566	320769	04 18.9	-55 03	9*9FF	
MCC 1566	331513	04 18.9	-55 03	9*9FF	
MCC 1566	117667	04 18.9	-55 03	9*9FF	
MCC 1566	112176	04 18.9	-55 04	9*9FF	
166848	04 21.1	+54 52	9*9F		
165227	04 21.1	+54 52	9*9F		
174613	04 26.1	+64 48	9*9FF	1	
MCC 1705	181113	05 26.1	+64 48	9*9FF	1
MCC 1705	165110	04 26.9	+54 45	9*9F	1

SC 2.016	SC 2.014	SC 2.014	SC 2.014	SC 2.014
217168	04 26.9	*54 85	*57 53	9*9FF
179237	04 27.1	*71 86	9*9FF	
179241	04 27.1	*71 86	9*9FF	
190510	04 27.8	*63 30	9*9FF	
192660	04 27.8	*63 30	9*9FF	
640120	04 26.1	*18 01	9*9F	
646704	04 26.1	*18 01	9*9F	
737030	04 26.1	*18 00	9*9F	
761993	04 26.1	*18 00	9*9F	
166547	04 26.2	*17 53	9*9FF	
640120	04 26.1	*17 53	9*9FF	
646704	04 26.1	*17 53	9*9FF	
737030	04 26.1	*18 00	9*9F	
150160	04 26.7	*18 01	9*9FF	
152112	04 26.7	*18 01	9*9FF	
154000	04 26.7	*18 01	9*9FF	
641025	04 26.8	*17 54	9*9F	
648862	04 26.8	*17 54	9*9F	
152117	04 29.1	*18 10	9*9FF	
154066	04 29.1	*18 10	9*9FF	
743689	04 29.2	*18 03	9*9F	
745053	04 29.2	*18 03	9*9F	
733701	04 29.3	*17 55	9*9F	
179961	04 29.3	*17 55	9*9FF	
157868	04 29.7	*24 18	9*9FF	
160743	04 29.7	*24 18	9*9FF	
152102	04 30.4	*22 91	9*9F	
152799	04 30.4	*22 37	9*9F	
217772	04 36.5	*50 15	9*9F	
220519	04 36.5	*50 15	9*9F	
LH120-4132	04 37.5	*50 15	9*9F	
210363	04 37.5	*50 15	9*9F	
220902	04 37.5	*50 15	9*9F	
157222	04 38.4	*25 40	9*9FF	
160352	04 38.4	*25 40	9*9FF	
157206	04 38.7	*25 34	9*9FF	
159951	04 39.6	*40 01	3*3SS	
CRL 616	179588	04 39.6	*40 01	3*3SS
CRL 616	182292	04 39.6	*40 01	3*3SS
NCC 1672	593952	04 41.9	-37 35	9*9FF
NCC 1672	602378	04 41.9	-37 35	9*9FF
B 026	223265	04 51.5	*30 30	9*9F
179942	04 51.5	*30 30	9*9F	
B 026	259135	04 51.5	*30 30	9*9F
261295	04 51.5	*30 30	9*9F	
105434	04 52.1	*30 33	9*9F	
190726	04 52.1	*30 33	9*9F	
103150	04 52.2	*69 27	9*9FF	
191174	04 52.2	*69 27	9*9FF	
179162	04 52.6	*30 28	9*9F	
81906	04 52.6	*30 28	9*9F	
325623	04 52.6	*30 34	9*9F	
258939	04 52.6	*30 34	9*9F	
SCH0 0136	270962	05 32.8	-95 34	9*9F
THE? ORI	194087	05 32.8	-95 35	9*9F
ST 36	194285	05 32.8	-95 26	9*9F
ST 36	210927	05 32.1	-71 06	9*9F
ST 36	222302	05 32.9	-95 27	3*3SS
THE? ORI	228851	05 32.5	-67 83	9*9FF
THE? ORI	279185	05 31.9	-95 27	3*3SS
THE? ORI	287087	05 32.7	-71 03	3*3SS
BADGAIN	162957	05 31.2	-21 59	9*9F
BADGAIN	165776	05 31.2	-21 59	9*9F
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	765221	05 31.2	-21 59	9*9F
BADGAIN	162954	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162953	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162954	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162953	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162954	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162953	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162954	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162953	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25.5	-69 41	3*3SS
BADGAIN	456367	05 25.9	-66 08	3*3SS
BADGAIN	465776	05 25.9	-66 08	3*3SS
BADGAIN	710358	05 31.2	-21 59	9*9F
BADGAIN	729560	05 31.2	-21 59	9*9F
BADGAIN	162954	05 32.1	-71 06	9*9F
BADGAIN	169227	05 32.1	-71 06	9*9F
BADGAIN	180133	05 32.5	-67 83	9*9FF
BADGAIN	187480	05 32.5	-67 83	9*9FF
BADGAIN	206041	05 25		

NGC 2276											
221865	06	10.6	+78	22	9+9F						
222658	06	10.6	+78	22	9+9F						
223825	06	10.6	+78	22	9+9F						
224805	06	10.6	+78	22	9+9F						
005600	06	11.0	+12	23	9+9F						
008313	06	11.0	+12	23	9+9F						
230439	06	13.6	+22	15	9+9F						
231783	06	13.8	+22	15	9+9F						
786222	06	14.2	-21	21	9+9F						
790236	06	14.2	-21	21	9+9F						
791936	06	14.2	-21	21	9+9F						
248164	06	14.3	+22	10	9+9F						
265665	06	14.3	+22	10	9+9F						
270147	06	14.3	+22	10	9+9F						
280123	06	14.3	+22	28	9+9F						
270149	06	14.3	+22	28	9+9F						
250318	06	14.7	+22	28	9+9F						
260894	06	14.7	+22	28	9+9F						
242673	06	15.0	+22	15	9+9F						
281090	06	15.0	+22	15	9+9F						
224968	06	17.6	-10	37	9+9F						
279947	06	17.6	-10	37	9+9F						
303849	06	17.6	-10	37	9+9F						
242673	06	17.6	-10	37	9+9F						
223900	06	21.0	-39	50	3+9SS						
226644	06	21.0	-39	50	3+9SS						
PX 233-16.1	06	25.0	-25	21	3+9SS						
PX 233-16.1	06	25.0	-25	21	3+9SS						
243838	06	36.4	+08	47	9+9F						
251107	06	38.4	+09	32	9+9F						
262695	06	38.4	+09	32	9+9F						
303672	06	39.0	-38	82	9+9F						
259383	06	40.4	-50	55	9+9F						
262713	06	40.4	-50	55	9+9F						
0434	05	39.8	-69	37	9+9F						
263706	05	39.8	-69	37	9+9F						
197835	05	40.2	-69	80	9+9F						
193915	05	40.2	-69	80	9+9F						
195287	05	40.4	-69	86	9+9F						
198627	05	40.4	-69	86	9+9F						
236066	05	40.5	-69	86	9+9F						
236021	05	40.5	-69	86	9+9F						
225215	05	43.0	-00	13	9+9F						
258852	05	43.0	-00	13	9+9F						
279154	05	43.0	-00	13	9+9F						
219007	05	47.6	-69	43	3+9SS						
211951	05	47.6	-69	43	3+9SS						
767394	05	53.1	-03	23	9+9F						
167247	05	57.9	-52	28	9+9F						
188229	05	57.9	-52	28	9+9F						
207059	05	58.0	-75	40	3+9SS						
209407	05	58.0	-75	40	3+9SS						
CCK 243-25.1	06	00.4	-37	25	3+9SS						
216606	06	00.4	-37	25	3+9SS						
239161	06	04.5	+19	26	9+9F						
264823	06	04.5	+19	26	9+9F						
279030	06	04.5	+19	26	9+9F						
215426	06	05.6	+20	31	9+9F						
240726	06	05.6	+20	31	9+9F						
275020	06	05.6	+20	31	9+9F						
288738	06	01.6	+20	40	9+9F						
209715	06	10.8	+78	27	9+9F						
LBN 1074	07	10.5	+81	51	9+9F						





NCC 3115	886698	10 02.7	-07 28	9*9F		VHE 408	581194	10 33.9	-58 59	9*9FF	BADGAIN
NCC 3115	883209	10 04.9	-56 58	9*9FF	BADGAIN		581151	10 36.1	-64 31	9*9F	BADGAIN
NCC 3115	892408	10 04.9	-56 58	9*9FF	BADGAIN		550221	10 36.1	-64 31	9*9FF	BADGAIN
NCC 3115	863766	10 12.8	-28 37	9*9F			573912	10 36.1	-64 31	9*9FF	BADGAIN
NCC 3175	866510	10 12.8	-28 37	9*9F			576676	10 36.1	-64 31	9*9FF	BADGAIN
NCC 3175	886488	10 12.8	-28 37	9*9F	BADGAIN		576749	10 36.1	-64 31	9*9FF	BADGAIN
NCC 3147	278902	10 12.7	-73 39	9*9FF		VHE 40A	579419	10 36.1	-64 31	9*9FF	BADGAIN
NCC 3147	281646	10 12.7	-73 39	9*9FF	BADGAIN		619797	10 36.5	-58 52	9*9F	BADGAIN
NCC 3177	825942	10 13.8	+21 22	9*9F		VHE 40A	580594	10 36.5	-58 52	9*9FF	BADGAIN
NCC 3177	826762	10 13.8	+21 22	9*9F	BADGAIN		571103	10 36.6	-58 52	9*9FF	BADGAIN
VHE 35	524758	10 14.0	-60 03	9*9FF		NMSI 285-00/1	579222	10 35.3	-58 38	9*9FF	BADGAIN
VHE 35	580806	10 14.0	-60 03	9*9FF	BADGAIN		580835	10 35.7	-57 45	9*9FF	BADGAIN
NCC 3198	NR18-NCC3199	10 15.2	-57 40	9*9F	BADGAIN		580889	10 36.2	-53 66	9*9F	BADGAIN
NCC 3198	NR18-NCC3199	10 15.2	-57 40	9*9F	BADGAIN		352417	10 35.7	-53 66	9*9F	BADGAIN
NCC 3198	500056	10 15.2	-57 40	9*9F	BADGAIN		367132	10 36.2	-41 57	9*9FF	BADGAIN
VHE 35	510451	10 16.6	-60 39	9*9F		WR22-NC2312	531372	10 39.4	-59 25	9*9F	BADGAIN
VHE 35	5580072	10 16.6	-60 39	9*9F	BADGAIN		531329	10 39.4	-59 25	9*9F	BADGAIN
NCC 3198	340657	10 16.9	+45 48	9*9FF		WR23-AMON	529257	10 39.7	-58 31	9*9F	BADGAIN
NCC 3198	565896	10 20.6	-58 53	9*9FF	BADGAIN		531804	10 39.7	-58 31	9*9F	BADGAIN
NCC 3226	810873	10 20.7	+20 08	9*9F		WR23-AMON	531835	10 40.8	+25 11	9*9FF	BADGAIN
NCC 3226	821476	10 20.7	+20 08	9*9F	BADGAIN		481192	10 40.5	+36 06	9*9FF	BADGAIN
WRAY 19.22	527222	10 22.3	-57 33	9*9FF	BADGAIN		489136	10 40.5	+36 06	9*9FF	BADGAIN
WRAY 19.22	551787	10 22.3	-57 33	9*9FF	BADGAIN		506135	10 40.5	+59 20	9*9FF	BADGAIN
VHE 36	489671	10 22.4	-57 38	9*9FF	BADGAIN		508882	10 40.5	-59 20	9*9FF	BADGAIN
VHE 36	922991	10 22.4	-57 38	9*9FF	BADGAIN		610234	10 40.8	+25 11	9*9FF	BADGAIN
VHE 36	533575	10 22.5	-57 38	9*9FF	BADGAIN		620835	10 40.8	+25 11	9*9FF	BADGAIN
VHE 36	583161	10 22.5	-57 39	9*9FF	BADGAIN		611566	10 41.0	+15 08	9*9F	BADGAIN
VHE 36	568651	10 22.9	-57 32	9*9FF	BADGAIN		505627	10 41.0	-59 21	9*9FF	BADGAIN
IC 2574	304770	10 28.7	+68 41	9*9FF		THE CAR	525253	10 41.0	-59 21	9*9FF	BADGAIN
IC 2574	349666	10 28.7	+68 41	9*9FF	BADGAIN		525539	10 41.1	-59 16	9*9FF	BADGAIN
NCC 3256	862182	10 25.7	-43 39	9*9F		THE CAR	532201	10 41.1	-59 16	9*9FF	BADGAIN
NCC 3256	885888	10 25.7	-43 39	9*9F	BADGAIN		843016	10 41.3	+11 58	9*9F	BADGAIN
NCC 3256	492790	10 25.7	-43 39	9*9F		HOFFL 06	550811	10 41.4	-60 00	9*9FF	BADGAIN
NCC 3256	494728	10 25.7	-43 39	9*9F	BADGAIN		536659	10 41.2	-64 08	31S	VHE 36
NCC 3256	495551	10 29.5	-57 47	9*9FF	BADGAIN		501331	10 41.2	-64 08	31S	VHE 36
NCC 3281	886676	10 29.6	-38 36	9*9F		THE CAR	502021	10 41.3	+11 58	9*9F	BADGAIN
VHE 39	578812	10 31.6	-59 25	9*9FF	BADGAIN		843016	10 41.3	+11 58	9*9F	BADGAIN
VHE 39	581776	10 31.6	-59 25	9*9FF	BADGAIN		521606	10 41.6	-59 11	9*9FF	BADGAIN
VHE 38	518877	10 31.9	-61 51	9*9FF		HOFFL 06	550811	10 41.6	-59 11	9*9FF	BADGAIN
VHE 38	539619	10 32.4	-61 37	9*9F		HOFFL 06	506921	10 41.6	-59 20	9*9FF	BADGAIN
VHE 38	545721	10 32.4	-61 37	9*9F		HODFL 06	525930	10 41.6	-59 20	9*9FF	BADGAIN
VHE 38	554380	10 32.4	-61 37	9*9F		HOFFL 06	568639	10 41.6	-59 26	9*9FF	BADGAIN
VHE 38	531211	10 32.4	-61 37	9*9F		HOFFL 06	507117	10 41.6	-59 28	9*9FF	BADGAIN
VHE 38	549436	10 32.4	-61 37	9*9F		HOFFL 06	516133	10 41.6	-59 19	9*9FF	HODFL 06
VHE 38	551180	10 32.4	-61 37	9*9F		HOFFL 06	570613	10 41.7	-59 19	9*9FF	HODFL 06
VHE 38	555903	10 32.4	-61 37	9*9F		HOFFL 06	548157	10 41.7	-59 19	9*9FF	HODFL 06
VHE 38	498686	10 32.5	-58 10	9*9FF		HOFFL 06	548128	10 41.7	-59 19	9*9FF	HODFL 06
VHE 38	500652	10 32.5	-58 10	9*9FF		HOFFL 06	501707	10 41.7	-59 11	9*9FF	HODFL 06
VHE 38	519468	10 32.6	-46 21	9*9FF		HOFFL 06	515931	10 42.1	-59 11	9*9FF	HODFL 06
VHE 38	524140	10 32.6	-46 21	9*9FF		HOFFL 06	515931	10 42.1	-59 11	9*9FF	HODFL 06
VHE 40R	611169	10 33.9	-18 19	9*9FF		HOFFL 06	515931	10 42.1	-59 11	9*9FF	HODFL 06



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NGC 4138	12 25.2	01 13 17	9*9FF		12 55.9	-76 51	9*9FF	1
NGC 4149	06 17 02	12 25.0	01 18 22	9*9F	25 99 09	12 56.0	-76 54	9*9F
NGC 4149	08 55 36	12 25.0	01 18 22	9*9F	26 54 77	12 56.0	-76 54	9*9F
NGC 4150	09 14 53	12 26.0	01 17 22	9*9FF	1 05 91 0	12 56.0	-77 19	9*9FF
NGC 4150	09 17 07	12 26.0	01 17 22	9*9FF	1 47 06 6	12 56.0	-77 19	9*9FF
NGC 4150	02 04 26	12 28.2	01 41 55	9*9F	24 08 19	12 56.1	-77 07	9*9F
NGC 4150	02 27 78	12 28.2	01 41 55	9*9F	25 60 55	12 56.1	-77 07	9*9F
NGC 4150	03 03 01	12 28.3	01 12 30	9*9F	26 09 68	13 00.5	-77 19	9*9F
NGC 4150	04 15 57	12 28.3	01 12 40	9*9F	26 56 71	13 00.5	-77 19	9*9F
NGC 4150	04 25 27	12 28.3	01 20 30	9*9F	1 00 61 5	13 01.8	-77 37	9*9FF
NGC 4150	05 56 58	12 28.6	01 20 30	9*9F	1 06 09 1	13 01.8	-77 37	9*9FF
NGC 4159	07 21 03	12 33.5	+26 14	9*9FF	1 56 33 3	13 02.5	-49 12	9*9F
NGC 4159	08 04 14	12 33.5	+26 14	9*9FF	1 57 62 0	13 02.5	-49 12	9*9F
NGC 4165	08 76 79	12 33.9	+26 16	9*9F	25 96 00	13 02.6	-49 12	9*9F
NGC 4165	05 10 19	12 33.9	+26 16	9*9FF	26 58 67	13 02.6	-77 40	9*9F
NGC 4166	04 25 04	12 34.3	+13 26	9*9FF	25 98 04	13 03.0	-77 31	9*9F
NGC 4169	04 08 04	12 34.3	+13 26	9*9FF	26 60 63	13 01.0	-77 31	9*9F
NGC 4169	04 31 29	12 36.7	-00 15	9*9FF	3 49 06 6	13 04.6	+67 58	9*9FF
NGC 4169	06 08 02	12 37.0	+61 53	9*9FF	3 77 09 7	13 04.6	+67 58	9*9FF
NGC 4169	05 10 19	12 37.0	+61 53	9*9FF	5 98 62 5	13 04.9	-65 02	9*9F
NGC 4169	05 21 36	12 39.7	+32 49	9*9F	6 01 17 2	13 08.9	-65 02	9*9F
NGC 4171	02 41 04	12 39.7	+32 49	9*9F	6 36 05 2	13 08.6	+37 19	9*9FF
NGC 4171	06 21 07	12 39.7	+32 49	9*9F	6 36 48 7	13 08.6	+37 19	9*9FF
NGC 4171	02 21 07	12 39.7	+32 49	9*9F	6 82 98 4	13 11.1	+36 52	9*9FF
FIT. N	1 46 05	12 41.0	-78 32	9*9FF	5 37 42 5	13 11.1	+36 52	9*9FF
FIT. N	1 49 05	12 41.0	-78 32	9*9FF	6 69 41 6	13 13.6	+42 10	9*9FF
FIT. N	2 16 47	12 41.2	-78 32	9*9FF	6 81 17 9	13 13.6	+42 10	9*9FF
FIT. N	1 06 08	12 41.2	-78 32	9*9FF	6 85 01 2	13 15.3	-57 52	9*9F
NGC 4156	5 24 08 5	12 41.5	+32 26	9*9FF	5 87 25 5	13 15.3	-57 52	9*9F
NGC 4156	5 27 62 9	12 41.5	+32 26	9*9FF	6 52 89 7	13 15.3	-62 26	9*9FF
NGC 4166	5 41 78 7	12 45.9	-01 02	3 01 55	5 00 01 6	13 16.2	-20 37	9*9FF
NGC 4166	5 42 37 3	12 45.9	-01 02	3 01 55	6 46 01 2	13 16.2	-20 37	9*9FF
NGC 4172	4 09 23 3	12 48.0	+25 16	9*9FF	5 55 51 1	13 19.1	-36 27	9*9FF
NGC 4172	5 49 19 0	12 48.0	+25 16	9*9FF	5 59 01 7	13 19.1	-36 22	9*9FF
NGC 4172	5 16 55 0	12 48.5	+41 24	9*9FF	5 60 59 9	13 22.5	-42 85	9*9F
NGC 4172	5 35 08 3	12 48.5	+41 24	9*9FF	5 66 00 6	13 22.5	-42 45	9*9FF
NGC 4172	2 26 27 4	12 50.1	-76 53	9*9F	5 68 02 9	13 22.5	-42 45	9*9F
NGC 4172	2 26 04 5	12 50.1	-76 53	9*9F	5 70 32 5	13 22.5	-42 45	9*9F
NGC 4172	5 43 32 0	12 50.4	+11 30	9*9FF	5 89 79 8	13 22.5	-42 45	9*9FF
NGC 4172	5 49 56 9	12 50.4	+11 30	9*9FF	6 1 93 70	13 22.6	-10 54	3 01 5
A 35	5 30 28 9	12 51.0	-22 35	9*9F	6 1 95 66	13 22.6	-10 54	3 01 5
A 35	1 45 71 2	12 51.0	-76 25	9*9FF	5 82 32 7	13 24.7	-41 13	9*9F
L T 5	1 07 67 3	12 51.0	-76 25	9*9FF	5 86 02 1	13 24.7	-41 13	9*9F
L T 5	1 46 67 3	12 53.1	-42 10	9*9F	5 92 07 1	13 27.1	-41 13	9*9F
NGC 4162	5 30 36 3	12 53.1	-26 10	9*9F	5 93 51 2	13 27.1	-17 42	9*9FF
NGC 4162	5 00 00 6	12 54.3	+21 57	9*9FF	6 2 66 85	13 27.1	-17 42	9*9FF
NGC 4162	5 01 03 8	12 54.3	+21 57	9*9FF	6 0 65 3	13 27.7	+58 41	9*9FF
UGC 4058	2 39 55 0	12 54.4	+57 09	9*9F	6 56 00 3	13 27.7	+58 41	9*9FF
UGC 4058	2 39 56 0	12 54.4	-77 08	9*9FF	6 60 07 1	13 27.7	+58 41	9*9FF
UGC 4058	3 01 33 4	12 54.4	-77 08	9*9FF	6 61 39 1	13 27.8	+58 41	9*9FF
UGC 4058	1 02 20 3	12 54.4	-77 08	9*9FF	6 66 56 9	13 27.8	+58 41	9*9FF
UGC 4058	1 02 21 0	12 54.4	-77 08	9*9FF	6 71 36 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 73 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 75 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 76 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 77 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 78 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 79 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 80 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 81 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 82 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 83 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 84 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 85 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 86 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 87 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 88 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 89 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 90 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 91 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 92 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 93 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 94 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 95 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 96 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 97 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 98 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	6 99 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 00 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 01 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 02 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 03 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 04 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 05 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 06 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 07 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 08 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 09 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 10 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 11 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 12 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 13 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 14 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 15 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 16 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 17 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 18 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 19 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 20 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 21 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 22 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 23 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4	-77 08	9*9FF	7 24 03 7	13 27.8	+58 41	9*9FF
R A I C A I N	1 02 21 0	12 54.4						

623506	14 57.7	-48 06	9*9F		707567	16 16.4	-57 17	9*9F		222365	17 11.8	-77 89	9*9FF				
626249	14 57.7	-48 06	9*9F		710703	16 16.4	-57 17	9*9F		281766	17 11.8	-77 89	9*9FF				
146164	14 59.3	-63 12	9*9FF		156123	16 18.4	-89 59	9*9FF	1	BADGAIN							
146075	14 59.3	-63 12	9*9FF		177094	16 18.4	-89 59	9*9FF	1	BADGAIN							
146301	14 59.5	-72 26	9*9F		MISL 312-01/2	16 20.6	-51 25	9*9F		258081	17 11.8	-77 89	9*9FF				
146537	14 59.5	-72 26	9*9F		MISL 312-01/2	16 20.6	-51 25	9*9F		771049	17 12.3	-62 46	9*9F				
146711	15 00.5	-72 15	9*9F		143396	16 24.0	-24 32	9*9F	1	BADGAIN							
146929	15 00.5	-72 15	9*9F	1	143502	16 24.2	-24 22	9*9F	1	BADGAIN							
601669	15 04.6	-01 18	9*9F		MCG 6101	16 30.2	+19 56	9*9F		247067	17 14.9	-77 06	9*9FF				
MCG 5850	15 04.6	-01 18	9*9F		MCG 6101	16 30.2	+19 56	9*9F		251842	17 14.9	-77 06	9*9FF				
MCG 5866	390125	15 05.1	+55 57	9*9FF	675382	16 30.2	+19 56	9*9F		260190	17 14.9	-77 06	9*9FF				
MCG 5866	410610	15 05.1	+55 57	9*9FF	683295	16 30.2	+19 56	9*9F		268624	17 14.9	-77 06	9*9FF				
MCG 5866	499000	15 05.1	+55 57	9*9FF	170227	16 30.6	-67 02	3*3S	1	MISL 351-00/4	193643	17 16.6	-35 25	9*9FF			
MCG 5866	505273	15 05.1	+55 57	9*9FF	TAU SCO	149060	16 32.8	-24 07	3*1S	1	BADGAIN						
MCG 5866	637220	15 05.3	-51 27	9*9F	149100	16 34.4	-10 29	3*1S		MISL 351-00/4	175554	17 16.6	-35 25	9*9FF			
MCG 5866	645409	15 05.3	-51 27	9*9F	149700	16 34.5	-16 06	9*9FF	1	BADGAIN							
MCG 9719	36016	15 08.2	+67 23	9*9FF	149654	16 34.5	-46 06	9*9FF	1	BADGAIN							
MCG 9515	153173	15 10.0	-58 57	9*9F	1	BADGAIN	172775	16 36.3	-86 07	9*9FF		MISL 348-01/1	695048	17 16.9	-38 54	9*9F	
MCG 59017	410022	15 14.6	+56 30	9*9FF	182077	16 36.3	-86 07	9*9FF		BADGAIN							
MCG 59017	423152	15 14.6	+56 30	9*9FF	172196	16 36.3	-86 08	9*9FF	1	BADGAIN							
MCG 59017	449012	15 14.6	+56 30	9*9FF	176704	16 36.3	-86 08	9*9FF	1	BADGAIN							
MCG 59017	49512	15 14.6	+56 30	9*9FF	677384	16 36.5	-45 35	9*9F		BADGAIN							
MCG 59017	498004	15 14.6	+56 30	9*9FF	695217	16 36.5	-85 35	9*9F		BADGAIN							
MCG 59017	146903	15 14.8	-56 29	9*9FF	1	BADGAIN	631840	16 41.3	+36 56	9*9F		191411	17 17.3	-35 46	9*9FF		
MCG 5929	540948	15 20.3	+41 51	3*3S	VHE 74	778679	16 45.1	-48 00	9*9F		BADGAIN						
MCG 5929	548666	15 24.3	+41 51	3*3S	VHE 74	719317	16 45.1	-48 00	9*9F		BADGAIN						
MCG 5962	620117	15 30.2	+16 46	9*9F	MCG 6215	754393	16 46.0	-58 55	9*9F		BADGAIN						
MCG 5962	661669	15 34.2	+16 46	9*9F	MCG 6215	757136	16 46.0	-58 55	9*9F		161072	17 19.2	-57 57	9*9FF			
MCG 5972	145729	15 40.7	-53 57	9*9FF	1	BADGAIN	721071	16 48.4	-59 08	9*9F		186012	17 19.2	-57 57	9*9FF		
MCG 5967	187690	15 40.7	-53 57	9*9FF	1	BADGAIN	724416	16 48.4	-59 08	9*9F		246674	17 25.6	-76 32	9*9FF		
MCG 5967	674654	15 41.9	-75 31	9*9F	MCG 6221	754984	16 48.4	-59 08	9*9F		BADGAIN						
MCG 5967	688569	15 41.9	-75 31	9*9F	MCG 6221	758307	16 48.4	-59 08	9*9F		251653	17 25.8	-76 32	9*9FF			
MCG 5967	691312	15 41.9	-75 31	9*9F	1	BADGAIN	169487	16 48.7	+05 04	9*9F		263532	17 25.8	-76 32	9*9FF		
MCG 5967	161998	15 45.0	-54 33	9*9FF	1	BADGAIN	161216	16 54.7	-50 32	9*9FF		782589	17 29.8	-33 36	9*9F		
MCG 5967	167487	15 45.0	-54 33	9*9FF	1	BADGAIN	163960	16 54.7	-50 32	9*9FF		785336	17 30.0	-07 05	9*9FF		
MCG 5967	167291	15 49.2	-54 29	9*9FF	1	BADGAIN	170890	16 55.3	-46 03	9*9F		186065	17 30.0	-07 05	9*9FF		
MCG 6015	193035	15 50.7	+62 27	9*9F	1	BADGAIN	1724216	16 55.3	-46 03	9*9FF		203017	17 30.0	-07 05	9*9FF		
MCG 6015	497625	15 50.7	+62 27	9*9F	VHE 74	779837	16 55.5	-40 32	9*9F		BADGAIN						
MSH 15-57	152985	15 51.6	-53 09	9*9F	1	BADGAIN	772050	16 55.5	-40 32	9*9FF		175521	17 36.4	-56 54	9*9FF		
MSH 15-57	155729	15 51.6	-53 09	9*9F	1	BADGAIN	219092	16 56.0	+35 25	3*1SS		178012	17 37.7	-52 55	9*9FF		
MSH 15-57	162195	15 52.0	-52 35	9*9FF	1	BADGAIN	184009	16 56.0	+39 25	3*1SS		CALFIELD	177878	17 38.6	-40 55	9*9FF	
MSH 15-57	166710	15 52.0	-52 35	9*9FF	1	BADGAIN	1724216	16 58.0	-79 17	9*9FF		188657	17 39.7	-44 55	9*9FF		
MSH 15-57	167680	16 03.2	-35 37	9*9F	1	BADGAIN	222168	16 58.0	-79 17	9*9FF		203017	17 40.3	-21 20	3*3SS		
MSH 15-57	169062	15 59.7	-53 02	9*9FF	1	BADGAIN	230403	16 58.0	-79 17	9*9FF		216341	17 40.3	-21 20	3*3SS		
MSH 15-57	170128	16 03.2	+66 38	9*9F	1	BADGAIN	280787	16 58.0	-79 17	9*9FF		262550	17 40.5	-40 55	9*9FF		
MSH 15-57	171763	16 03.2	+66 38	9*9F	1	BADGAIN	232377	16 59.4	-33 12	9*9FF		265302	17 40.5	-40 55	9*9FF		
WR 72	736357	16 03.2	+66 38	9*9F	1	BADGAIN	757171	17 11.0	-39 82	9*9F		CALFIELD	196898	17 41.2	-36 55	9*9FF	
WR 72	743020	16 03.2	-35 37	9*9F	1	BADGAIN	8 049	240610	16 59.4	-33 12	9*9FF		25156	17 41.9	-32 55	9*9FF	
WR 72	167680	16 06.5	-51 59	9*9FF	1	BADGAIN	8 049	173179	16 59.4	-33 12	9*9FF		261397	17 41.9	-32 55	9*9FF	
WR 72	170128	16 06.5	-51 59	9*9FF	1	BADGAIN	164978	17 02.9	-10 05	3*1S		175713	17 42.2	-64 38	9*9FF		
WR 72	171763	16 13.5	-51 52	9*9FF	1	BADGAIN	185950	17 02.9	-10 05	3*1S		178857	17 42.2	-64 38	9*9FF		
WR 72	176300	16 13.5	-51 52	9*9FF	1	BADGAIN	701294	17 11.0	-39 82	9*9F		261262	17 41.4	-32 55	9*9FF		
WR 72	177462	16 13.8	-50 25	9*9F	1	BADGAIN	NGC 6180	21443	17 11.1	-72 27	9*9FF		268649	17 42.7	-44 30	9*9FF	
WR 72	175917	16 13.8	-50 25	9*9F	1	BADGAIN	M12 6140	28140	17 11.1	-72 27	9*9FF		203017	17 43.4	-20 20	1*1SS	
WR 72	163941	16 14.1	-40 17	9*9FF	1	BADGAIN	M12 6140	349267	17 11.1	-72 27	9*9FF		216740	17 43.1	-20 20	1*1SS	
WR 72	171144	16 15.9	-40 17	9*9FF	1	BADGAIN	M12 6140	311144	17 11.1	-72 27	9*9FF		161010	17 44.0	-24 24	9*9FF	

CALFIELD	17 44.0	-16 55	9*9FF		16 28.0	*23 27	3*15		19 07.9	-09 01	9*9FF		BADGAIN	
CALFIELD	201629	17 44.0	-12 55	9*9FF	1	16 25.7	*24 15	9*9F	261222	19 03.0	-04 54	9*9F		
CALFIELD	19403	17 44.0	-08 56	9*9FF	1	16 25.7	*24 15	9*9F	SS 033	19 09.4	-04 54	9*9F		
CALFIELD	191439	17 45.1	-08 56	9*9FF	1	16 27.3	*01 13	9*9F	SS 033	19 11.2	-54 45	9*9F		
CALFIELD	188625	17 45.1	-00 56	9*9FF	1	16 27.3	*01 13	9*9F	IC 4037	341740	19 12.0	-11 04	9*9FF	
CALFIELD	228715	17 50.0	+70 04	9*9FF		16 27.3	*01 13	9*9F	MIL 76	259072	19 12.0	+11 04	9*9FF	
MCG 6503	232011	17 50.0	+70 09	9*9FF		16 28.0	*22 01	9*9F	MIL 76	285332	19 12.0	+11 04	9*9FF	
MCG 6501	356502	17 50.0	+70 09	9*9FF		16 29.2	*26 53	3*3SS	MCG 6835	863095	19 15.0	-12 82	9*9F	
MCG 6503	386520	17 50.0	+70 09	9*9FF		16 29.2	*26 53	3*3SS	LDN 0723	243982	19 16.0	-19 06	9*9FF	
A 43	204775	17 51.2	+10 38	3*3SS		16 29.2	*26 53	3*3SS	LDN 0723	249278	19 16.0	-19 06	9*9FF	
PK 051-28.1	203210	17 52.3	+26 00	3*3SS		16 30.7	*37 18	9*9F	LDN 0723	257307	19 16.0	-19 06	9*9FF	
PK 051-28.1	205371	17 52.3	+28 00	3*3SS		16 31.7	*37 18	9*9F	NH 32A + B	251614	19 16.1	+10 56	9*9FF	
PK 053-24.1	201311	17 52.3	+28 00	3*3SS		16 39.1	*26 52	3*3SS	VT 2-2	240871	19 22.0	+00 10	3*3SS	
A 46	198721	17 58.6	+66 30	3*3SS		16 35.8	*28 00	9*9F	VT 2-2	253775	19 22.0	-00 10	3*3SS	
CALFIELD	NGC 6541	17 58.6	+66 30	3*3SS		16 36.2	*15 53	9*9FF	HH 32A + B	250666	19 22.0	-00 10	3*3SS	
NGC 6543	201075	17 58.6	+66 30	3*3SS		16 37.5	*11 59	9*9FF	HH 32A + B	253372	19 18.1	-10 56	9*9FF	
NGC 6543	357002	17 58.6	+66 30	3*3SS		16 38.7	*08 08	9*9FF	HH 32A + B	310027	19 18.1	-10 56	9*9FF	
NGC 6543	360228	17 58.6	+66 30	3*3SS		16 39.1	*26 52	3*3SS	PK 056-14.1	250485	19 21.8	+11 24	9*9FF	
NGC 6543	200867	17 58.6	+66 30	3*3SS		16 39.1	*26 52	3*3SS	PK 056-14.1	236930	16 39.1	+00 10	3*3SS	
NGC 6543	364539	17 58.6	+66 30	3*3SS		16 39.1	*26 52	3*3SS	CALFIELD	262995	16 39.9	+04 20	9*9FF	
NGC 6543	367079	17 58.6	+66 30	3*3SS		16 41.1	*00 32	9*9FF	CALFIELD	263570	16 41.1	+00 32	9*9FF	
NGC 6543	369635	17 58.6	+66 30	3*3SS		16 41.6	*03 51	9*9F	MR 121	783554	16 42.3	-03 14	9*9FF	
NGC 6543	199113	17 58.6	+66 30	3*3SS		16 42.3	*03 14	9*9F	CALFIELD	271613	16 38.7	+08 08	9*9FF	
NGC 6543	206561	17 58.6	+66 30	3*3SS		16 43.0	*03 14	9*9F	PK 056-14.1	225162	16 39.1	+28 00	9*9F	
NGC 6543	200662	17 58.6	+66 30	3*3SS		16 43.5	*02 83	9*9F	PK 056-14.1	236331	16 43.5	-02 83	9*9F	
NGC 6543	210268	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	CALFIELD	263570	16 41.1	+00 32	9*9FF	
NGC 6543	284767	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	MR 121	783554	16 42.3	-03 14	9*9FF	
NGC 6543	293983	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	CALFIELD	291597	16 42.3	-03 14	9*9FF	
NGC 6543	326517	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	PK 056-0.0	259053	16 43.0	-02 83	9*9F	
NGC 6543	329066	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	NGC 6543	250662	17 58.6	+66 30	3*3SS	
NGC 6543	331223	17 58.6	+66 30	3*3SS		16 43.5	*02 84	9*9FF	NGC 6543	263331	16 43.5	-02 83	9*9F	
NGC 6543	333188	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	263570	16 47.6	+20 47	3*3SS	
NGC 6543	337296	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6699	326601	16 47.6	+01 49	9*9F	
NGC 6543	340635	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	256702	16 45.2	-01 50	9*9F	
NGC 6543	361990	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	262950	16 45.2	-01 50	9*9F	
NGC 6543	362386	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	229970	16 47.6	+20 47	3*3SS	
NGC 6543	362975	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	233202	16 47.6	+20 47	3*3SS	
NGC 6543	364147	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	233009	16 47.6	+20 47	3*3SS	
NGC 6543	364738	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	242799	16 47.6	+07 50	9*9F	
NGC 6543	365133	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	262204	16 45.2	+35 11	3*3SS	
NGC 6543	374340	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6543	239052	16 50.6	+01 11	9*9FF	
NGC 6543	375516	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6720	242005	16 50.8	+01 11	9*9FF	
NGC 6543	378869	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6720	224581	16 51.7	+32 58	3*3SS	
NGC 6543	378454	17 58.6	+66 30	3*3SS		16 47.6	*20 47	3*3SS	NGC 6720	233009	16 51.7	+35 11	3*3SS	
NGC 6543	210614	17 59.3	+66 40	9*9F		16 50.6	*32 58	9*9F	NGC 6543	207092	16 51.7	+32 58	9*9F	
NGC 6571	763161	18 09.6	+11 58	9*9F		16 52.3	*05 58	9*9F	NGC 6720	261026	16 52.3	+05 58	9*9F	
NGC 6574	766922	18 09.6	+11 58	9*9F		16 52.3	*05 58	9*9F	NGC 6720	243792	16 52.3	+05 58	9*9F	
NGC 6572	204185	18 09.7	+06 50	3*3SS		16 52.3	*05 58	9*9F	PK 078+8.1	289643	16 51.7	+32 58	3*3SS	
NGC 6572	238878	18 09.7	+06 50	3*3SS		16 52.3	*05 58	9*9F	PK 078+8.1	245753	16 50.0	+46 24	3*3SS	
CM 3-1	203791	18 15.2	+10 08	3*3SS		16 52.3	*05 58	9*9F	NGC 6749	210990	19 05.0	-63 56	9*9FF	
CM 3-1	230168	18 15.2	+10 08	3*3SS		16 52.3	*05 58	9*9F	NGC 6749	239270	18 55.6	+01 35	9*9FF	
CM 3-1	216009	18 19.0	+56 39	3*3SS		16 52.3	*05 58	9*9F	NGC 6749	242203	18 55.6	+01 35	9*9FF	
CM 3-1	257760	18 19.0	+56 39	3*3SS		16 52.3	*05 58	9*9F	NGC 6749	243792	18 55.6	+01 35	9*9FF	
CM 3-1	281956	18 19.0	+56 39	3*3SS		16 52.3	*05 58	9*9F	NGC 6749	271970	19 10.7	+16 18	3*3SS	
CM 3-1	222344	18 21.2	+74 11	9*9FF		16 52.3	*05 58	9*9F	NGC 6749	262297	19 10.7	+16 18	9*9FF	
CM 3-1	246611	18 21.2	+74 11	9*9FF		16 52.3	*05 58	9*9F	NGC 6749	270822	19 10.7	+16 18	9*9FF	
CM 3-1	194118	18 24.0	+11 41	9*9FF		16 52.3	*05 58	9*9F	NGC 6749	271970	19 10.7	+16 18	9*9FF	
CM 3-1	246611	18 24.0	+11 41	9*9FF		16 52.3	*05 58	9*9F	NGC 6749	270822	19 10.7	+16 18	9*9FF	
CM 3-1	246611	18 24.0	+11 41	9*9FF		16 52.3	*05 58	9*9F	NGC 6749	271970	19 10.7	+16 18	9*9FF	





D-083608  
C-026043

TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM  
OPTIONS IN EFFECT: LIST001,NOHEX 09/09/91 7:50:40.9 INPUT VOL=JJ0002 (LAST MOD-24OCT88) PAGE 1

C2148-T1 IRAS-DAX Chopped Photometric Channel 00010000 CPCFT1 : 489 observations RA : 00 to 07 h

TAPEMARK NO 0001 BLOCK LENGTHS: MIN=00160 MAX=00160 AVG=00160 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0002 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0003 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0004 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0005 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0006 BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0007 BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0008 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0009 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0010 BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0011 BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0012 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0013 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 0014 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM 09/09/91 7:50:40.9 INPUT VOL=JJ0002 (LAST MOD-24OCT88) PAGE 70

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0967 BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0968 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0969 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0970 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0971 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0972 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0973 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0974 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0975 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0976 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0977 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0978 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT  
TAPEMARK NO 0979 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

C2148-T2 IRAS-DAX Chopped Photometric Channel 00010000 CPCFT2 : 624 observations RA : 08 to 15 h

TAPEMARK NO 0980 BLOCK LENGTHS: MIN=00160 MAX=00160 AVG=00160 NUMBER OF BLOCKS=000001

TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM                    09/09/91 7:50:40.9 INPUT VOL=JJ0002 (LAST MOD=24OCT88) PAGE 160

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2227    BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2228    BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

C2148-T3 IRAS-DAX Chopped Photometric Channel    00010000 CPCFT3 : 395 observations RA : 16 to 23 h

TAPEMARK NO 2229    BLOCK LENGTHS: MIN=00160 MAX=00160 AVG=00160 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2230    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2231    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2232    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2233    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2234    BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2235    BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2236    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2237    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2238    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2239    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2240    BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001

D-283698  
C-028093

LECTURE V4.0 C.D.S. 18.04.89 16:53:15

2<sup>nd</sup> file (1<sup>st</sup> tape)

18.04.8

Lrec1= 80, Blksize= ~~2680~~,

Lecture partielle: 30 enreg. puis 1, tous les 1000

Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 180

LECTURE V4.0 C.D.S. 18.04.89 16:53:28

979<sup>th</sup> file (1<sup>st</sup> tape)

18.04.89

Lrec1= 80. Blksize= 2000.  
Lecture partielle: 30 enreg. puis 1, tous les 1000.  
Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 180

LECTURE V4.0 C.D.S. 18.04.89 16:56:41

981<sup>st</sup> file (1<sup>st</sup> tape)

18.04.89

Lrec1= 80. Blksize= 2080.  
Lecture partielle: 30 enreg. puis 1 ,tous les 1000.  
Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 180

LECTURE V4.0 C.D.S. 18.04.89 16:56:50

2228<sup>th</sup> file (1<sup>st</sup> type)

18.04.89

Lrec1= 80. Blksize= 2880.  
Lecture partielle: 30 enreg. puis 1, tous les 1000.  
Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 180

LECTURE V4.0 C.D.S. 18.04.89 16:59:35

2<sup>nd</sup> file (2<sup>nd</sup> tape)

18.04.8

Lrec1= 80. Blksize= 2800.  
Lecture partielle: 30 enreg. puis 1, tous les 1000.  
Conversion ASCII -> EBCDIC. (code ASCII détecte automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 144

LECTURE V4.0 C.D.S. 18.04.89 16:59:42

791<sup>st</sup> file (2<sup>nd</sup> tape)

• 8.04.89

Lrec1= 80. Blksize= 2880.

Lecture partielle: 30 enreg. puis 1 ,tous les 1000.

Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

Dernier enregistrement du fichier:

Nombre d'enregistrements = 180

LECTURE V4.0

C.D.S.

18.04.89 17:00:52

792<sup>nd</sup> fil (2<sup>nd</sup> tape)

18.04.89

Lrec1= 80, Blksize= 2880,

Lecture partielle: 30 enreg. puis 1, tous les 1000.

Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

1	2	3	4	5	6	7	8	9
1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890	1234567890
EXTENSION	= 'TABLE'	/ CPC (IRAS) list of observations on tape						
BITPIX	=	8 /						
NAXIS	=	2 / 2D table						
NAXIS1	=	40 / max number of characters per row						
NAXIS2	=	1508 / number of rows (observations)						
TFIELDS	=	8 / number of fields per row						
EXTNAME	= 'CPC-OBS'	/						
EXTVER	=	2 / Second version of the list						
TTYPE1	= 'OBJ.NAME'	/ astronomical name of object						
TBCOL1	=	1 / max 13 char						
IFORM1	= 'A13'	/						
TTYPE2	= 'TIME OBS'	/ time of observation						
TBCOL2	=	14 / 1 unit is about 31.6 sec time						
TFORM2	= 'I6'	/						
TUNIT2	= 'MICRO.YR'	/ fraction of year since 1983.0						
TTYPE3	= 'RAH'	/ Right Ascension; hour part						
TBCOL3	=	20 /						
TFORM3	= 'I3'	/						
TUNIT3	= 'HR'	/						
TTYPE4	= 'RAM'	/ Right Ascension; minutes and decimal fraction						
TBCOL4	=	23 /						
TFORM4	= 'F5.1'	/						
TUNIT4	= 'MIN'	/						
TTYPE5	= 'DECDSIGN'	/ Declination sign						
TBCOL5	=	28 /						

Dernier enregistrement du fichier:

Nombre d'enregistrements = 828

LECTURE v4.0 C.D.S. 18.04.89 16:53:15 2<sup>nd</sup> file (1<sup>st</sup> tape) C2A48 18.04.89 16:53:15 Page 1

Dernier enregistrement du fisher : COMMMENT START OF SCAN AT (COL,ROW)=( 5,26) TO (COL,ROW)=(20,49) IN 10 SECONDS .

Nombre d'enregistrements = 180



LECTURE V4: O

18.04.89 16:56:41

981 " like (1st tape)

१८

`lrec= 80. Blksiz= 2880.  
Lecture partielle: 30 enreg. puis 1 et tous les 1000.  
Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement)`

Derrière enregistrement du fichier.

卷之三

Dernier enregistrement du fichier :

Nombre d'enregistrements = 180



LECTURE V4.0 C.D.S. 18.04.89 16:59:42

Lrec1= 80, Blksize= 2880,

Lecture partielle: 30 enreg. puis les 1000.

Conversion ASCII -> EBCDIC. (code ASCII détecté automatiquement).

LECTURE V4.0 C.D.S. 18.04.89 16:59:42

791st file (2nd tape)

:

```

SIMPLE
BITPIX = 16 / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214 )
NAXIS = 3 / PIXEL VALUES: 2-BYTE TWO'S-COMPLEMENT INTEGERS
NAXIS1 =
NAXIS2 =
NAXIS3 =
CTYPE1 =
'RA
    3.58500E+02 / COORDINATE TRANSFORMATIONS:
CRPIX1 = 2.30000E+01 / OF PIXEL = { COLUMN - CRPIX1 ) * CDELT1
    -5.55556E-03 / Y OF PIXEL = ( ROW - CRPIX2 ) * CDELT2
CDELT1 = 'DEC
CTYPE2 =
CRVAL2 =
CRPIX2 = 5.82500E+01 / TRANSFORMATIONS BETWEEN (X,Y) AND (RA,DEC):
    2.80000E+01 / APPROXIMATE (FAR FROM THE CELESTIAL POLES):
CDELT2 = 5.55556E-03 / X = (CRVAL1 - RA) * COS(CRVAL2)
'LAMBDA
CDELT3 = 5.00000E+00 / Y = DEC - CRVAL2
CDELT4 = 5.00000E-05 / EXACT:
CRVAL3 = 5.00000E-05 / X = SIN(CRVAL1 - RA)*COS(DEC)
CDELT3 = 5.00000E-05 / Y = ( SIN(DEC) * COS(CRVAL2) ) -
BSCALE = 3.21897E-03 / ( COS(DEC) * SIN(CRVAL2) * COS(RA-CRVAL1) )
BZERO =
BUNIT =
'MJY / SR'
BLANK =
DATE-OBS = '29/07/83'
TIME-OBS = '06:32:37'
INSTRUME = 'IRAS CPC'
ORIGIN =
'ROG-GRON'
OBJECT =
'LDN 1253
COMMENT IRAS CPC RAW IMAGE :NO DEGLITCHING, NO GAINCORRECTION APPLIED.
COMMENT START OF SCAN AT (COL,ROW)=( 4,27 ) TO (COL,ROW)=( 13,37 ) IN 10 SECONDS.
Dernier enregistrement du fichier:
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Nombre d'enregistrements = 828

TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM  
 OPTIONS IN EFFECT: LIST001,NOHEX  
 PAGE 1

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C2148-T1 IRAS-DAX Chopped Photometric Channel
      BLOCK LENGTHS: MIN=00160 MAX=00160 AVG=00160 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0002
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0003
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0004
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0005
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0006
      BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0007
      BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0008
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0009
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0010
      BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0011
      BLOCK LENGTHS: MIN=11520 MAX=11520 AVG=11520 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0012
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0013
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001
SIMPLE = T / SIMPLE FITS FORMAT ( HEADER VERSION D1 850214) BITPIX = 16 / PIXEL VALUES: 2-BYT
TAPEMARK NO 0014
      BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001

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TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 7 : 50 : 40 . 9 INPUT VOL=JJ0002 (LAST MOD-24OCT88) PAGE 70  
 TAPEMARK NO 0967 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0968 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0969 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0970 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0971 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0972 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0973 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0974 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0975 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0976 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0977 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0978 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT  
 TAPEMARK NO 0979 BLOCK LENGTHS: MIN=14400 MAX=14400 AVG=14400 NUMBER OF BLOCKS=000001 16 / PIXEL VALUES: 2-BYT  
 C2148-T2 IRAS-DAX Chopped Photometric Channel 00010000 CPCFT2 : 624 observations RA : 08 to 15 h  
 TAPEMARK NO 0980 BLOCK LENGTHS: MIN=00160 MAX=00160 AVG=00160 NUMBER OF BLOCKS=000001

TAPESCAN 4.4 - TAPE ANALYSIS AND COPYING PROGRAM

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 7:50:40.9 INPUT VOL=JJ0002 (LAST MOD~24OCT88) PAGE 160

TAPEMARK NO 2227 BLOCK LENGTHS: MIN=14400 MAX=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2228 C2148-T3 IRAS-DAX Chopped Photometric Channel BLOCK LENGTHS: MIN=14400 MAX=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 00010000 CPCFT3 : 395 observations RA : 16 to 23 h

TAPEMARK NO 2229 BLOCK LENGTHS: MIN=00160 MAX=00160 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2230 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = AVG=11520 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2231 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2232 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2233 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2234 BLOCK LENGTHS: MIN=14400 MAX=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2235 BLOCK LENGTHS: MIN=14400 MAX=14400 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2236 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2237 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2238 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2239 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

SIMPLE = T / SIMPLE FITS FORMAT < HEADER VERSION D1 850214> BITPIX = 16 / PIXEL VALUES: 2-BYT

TAPEMARK NO 2240 BLOCK LENGTHS: MIN=11520 MAX=11520 NUMBER OF BLOCKS=000001

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\$EXE TPLIST BS

) INPUT PARAMETERS ARE: AS SR=1=1

TAPE NO. 1 FILE NO. 1  
RECORD 1 LENGTH 160  
C2148-T1 IRAS-DAX Chopped Photometric Channel  
Rvations RA : 01 to 07 h 00010000 CPCFT1 : 489 obse

\*\*\*\* JOB DONE.  
\$EXE TPLIST BS

) INPUT PARAMETERS ARE: AS SR=1=1 1 98

TAPE NO. 1 FILE NO. 980  
RECORD 1 LENGTH 160  
C2148-T2 IRAS-DAX Chopped Photometric Channel  
Rvations RA : 38 to 15 h 00010000 CPCFT2 : 624 obse

\*\*\*\* JOB DONE.  
\$EXE TPLIST BS

) INPUT PARAMETERS ARE: AS SR=1=1 1 2229

TAPE NO. 1 FILE NO. 2229  
RECORD 1 LENGTH 160  
C2148-T3 IRAS-DAX Chopped Photometric Channel  
Rvations RA : 16 to 23 h 00010000 CPCFT3 : 395 obse

\*\*\*\* JOB DONE.  
\$WE0 LPS

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NGC	2005	41621	12.4	-39	28	9*FFNGC	F0E5	418954	00	12.4	-39	28	9*9FFN						
3C 2154	505582	00	27.9	-33	32	9*FFNGC	U134	459723	00	27.9	-33	32	3*9FFN						
11 37.8	+40	26	9*FFNGC	31	536988	J1	37.8	+40	J1	26	9*FFNGC	561290	00						
PN 31	564423	11	37.8	+41	25	9*FFNGC	31	558495	01	39.5	+41	14	9*FFNGC						
9 39.5	+41	64	9*FFNGC	31	645768	00	39.5	+41	04	9*FFNGC	31	635943	03						
9*9FFN	31	00	39.5	+40	34	9*FFNGC	31	559929	00	39.6	+40	54	9*FFNGC						
751	00	39.6	+40	54	9*FFNGC	31	551882	00	39.6	+40	54	9*FFNGC	31						
9*9FFN	31	00	39.6	+41	00	9*FFNGC	31	552490	00	40.0	+41	01	9*9FFN						
6631	03	40.0	+41	00	9*FFNGC	31	552452	01	41.7	+41	01	9*9FFN	31						
9*9FFN	31	00	40.0	+41	00	9*FFNGC	31	558912	01	41.9	+41	01	9*9FFN						
E1-S15	11	41.4	+41	05	9*FFNGC	31	545416	01	40.4	+41	05	9*FFNGC	31						
50 9*9FFN	31	00	41.5	+41	04	9*FFNGC	31	578335	00	41.5	+41	04	9*9FFN						
567158	00	41.5	+41	04	9*FFNGC	31	571581	00	41.5	+41	04	9*9FFN	31						
41 74	9*FFNGC	31	00	41.9	+41	10	9*FFNGC	31	594196	01	41.5	+41	11	9*9FFN					
596359	JN	41.9	+41	11	9*FFNGC	31	598700	00	40.4	+41	05	9*9FFN	31						
*57 37 9*FFN	31	00	42.0	+41	15	9*FFNGC	31	598715	01	42.2	+41	16	9*9FFN						
50 50576	00	42.2	+41	16	9*FFNGC	31	502832	00	42.2	+41	15	9*FFNGC	31						
* 5 *41 22 9*9FFN	31	00	42.7	+41	38	9*FFNGC	31	549525	01	42.7	+41	22	9*9FFN						
51 1 525	00	42.7	+41	38	9*FFNGC	31	549525	01	42.7	+41	38	9*FFNGC	31						
42.7 +41 35 9*9FFN	31	00	42.7	+41	38	9*FFNGC	31	558701	01	42.7	+41	38	9*9FFN						
) 596377	JJ	43.2	+69	59	9*9F	603623	00	48.6	+69	03	9*9F	NGC 0300	00						
52.5 -37 57 9*9FFNGC	13	00	467957	10	52.5	-37	57	9*9FFACK	125-47.1	504246	00	57.3	+15	28	9*9F				
4 ACK	47.1	515226	36	57.3	+15	28	9*9F	IC 1613	489534	51	02.2	+01	51	9*9FFIC	1613				
1 62.2 *01 51 9*9FFTRC	10011	00	535972	01	33.8	+12	19	9*9FFTRC	10011	535335	01	42.5	+12	13	9*9FF				
FFNGC 04.14	523.59	JN	31	66.7	+35	27	9*9FFNGC	J434	525997	01	66.7	+35	27	9*9FFNGC	J474				
* 71 17.8 +33 63 9*9FFNGC	3474	00	521875	01	17.5	+13	15	9*9FFNGC	32	562058	01	17.5	+12	13	9*9FF				
7177	JJ	30.4	+30	38	9*9FFNGC	33	568364	01	30.4	+30	38	9*9FFNGC	33	562058	01				
5*9FFN 33	00	39.5	+30	39	9*9FFNGC	33	583024	01	31.0	+30	24	9*9FFNGC	33	562058	01				
5.2111	JJ	31.0	+30	24	9*9FFNGC	33	499347	01	31.0	+30	24	9*9FFNGC	33	562058	01				
31 9*9FFN	33	00	31.0	+30	24	9*9FFNGC	33	516817	01	31.0	+30	31.0	+30	526793	11				
61 13.6	JJ	31.0	+31	31	9*9FF	508758	01	31.0	+30	31	9*9FFNGC	33	526793	11	31.0	+30			
1 31 9*9FF	5	16.598	01	31.6	+30	31	9*9FFNGC	31	503268	01	31.6	+30	31	9*9FFNGC	31				
531291	61	34.4	+15	32	9*9FFNGC	31	534034	01	34.6	+15	32	9*9FFNGC	31	536778	01	37.5			
+15 39 9*9FFUGC	1176	00	541886	01	35	15	39	9*9FFNGC	9613	542644	01	32.0	-29	4.0	9*9FF	NGC 0628			
38 775414	01	38.4	-75	16	9*9F	NGC 65171	01	39.5	+51	19	9*9FF	NGC 65071	01	38.4	-75	16	9*9FF		
2 +51 19 9*9F	NGC 1651	00	531486	01	41.4	+13	23	9*9FFNGC	6660	535521	01	40.4	+13	23	9*9FFNGC	0			
7.6 1 -57 04 9*9FF NGC	0777	00	556384	01	37.4	+31	11	9*9F	NGC 0777	564214	01	57.4	+31	11	9*9FF	NGC 0			
7.64	587337	JJ	38.6	+28	36	9*9FFNGC	31	579581	01	38.4	+28	36	9*9FFNGC	31	579532	02			
19.4 +42 17 9*9F	NGC 1891	00	581675	02	19.4	+42	07	9*9F	NGC 1891	584049	01	31.6	+3	31.6	+3	31.6			
3C 2891	142353	JJ	19.4	+42	07	9*9FFNGC	32	581655	02	24.5	+33	21	9*9FFNGC	32	583417	01			
12 24.3 +33 21 9*9F	NGC 1925	00	586161	02	24.3	+33	21	9*9F	NGC 1925	588904	02	24.3	+33	21	9*9FF	NGC 0			
U6C 2435	587334	JJ	31.0	+29	32	9*9F	UGC 2035	591451	02	31.5	+29	32	9*9FF	NGC 1986	59577	01			
5 12 31.6 -39 15 9*9F	MAFFE1	1	32.6	+59	9*9FFMAFFE1	2	32.6	+59	9*9FFMAFFE1	1	215916	02	32.6	+59	26	9*9FF			
2 12 43.7 -62 43	9*9F	NGC 1197	00	558293	02	44.0	-30	21268	02	38.1	+59	23	9*9FF	631060	02	48.6	+69	03	
2 394 02 51.0	2	+41	23	9*9F	NGC 1140	00	5682418	02	52.1	-10	14	9*9F	NGC 1140	585556	02	52.0	-10	1	
4 9*9F	ACK	25.5	-31.1	49.7	00	52.2	-44	22	9*9F	ACK	255-59.1	02	55.2	-44	22	9*9F			
15 1139 12 59.4	+61	16	9*9F	NGC 1169	00	516982	03	50.0	+46	11	9*9FFNGC	1169	516873	13	53.5	+58	19	9*9FF	NGC 1291
71 9*9FF	497737	3	15.6	-41	18	9*9FFNGC	1291	516873	13	15.6	-41	18	9*9FF	198959	516.5	16.5	16.5	16.5	+

```
INCP  
SNOP  
FNOP  
STOP  
$EXE TPLIST ES  
-----LIST OF GATL0UT1-----  
  
INPUT PARAMETERS ARE: AS SR=1=1  
  
TAPE NO. 1 FILE NO. 1  
RECORD 1 LENGTH 150  
C2148-T1 IRAS-DAX Chopped Photometric Channel  
Rvations PA: 0 to 37 h  
***** JUS DONE.  
$EXE TPLIST ES  
  
INPUT PARAMETERS ARE: AS SR=1=1 1 1 342 J  
  
TAPE NO. 1 FILE NO. 342 J  
RECORD 1 LENGTH 3168  
XTENSION = *TABLE * CPC (IRAS) list of observations on tape  
8 /  
ble  
er row NAXIS1 = NAXIS 4 J / max number of characters  
TFIELDS = 8 / number of fields per row  
-05-  
econd version of the list  
TTYPE1 = *OBJ-NAME astronomical name of object  
TBCOL1 = 1 / max 13 char  
TTYPE2 = *TIME OBS / time of observation  
ton TBCOL2 = 14 / 1 unit is second 31.6 sec time  
MICRO-YR fraction of year since 1983.0  
TUNIT2  
tom hour TTYPE3 = *RAH 23 / Right Ascens  
TBCOL3 = 1 /  
TTYPE4 = *RAM 23 / Right As  
tension minutes and decimal fraction TBCOL4 = /  
TFORM4 = *F5.1 /  
TUNIT4 = *MIN  
inatation sign TFORM5 = *A2 TBCOL5 = *DECDSIGN / Decl  
CD / Declination; degree part (unsigned)  
TUNIT6 = *DEG TFORM6 = 28 /  
*DEC M / Declination; minutes part  
TUNIT7 = *ARC-MIN TFORM7 = 13 /  
TBCOL7 = 3 /  
***** TYPES  
* RASTER * / type of raster scan used  
TBCOL8 = 13 /  
* 35 /  
* 9*9FE*, )  
t = *11/14/85, ORIGIN = *OS-BRON / creation date of this file  
TITLE = *CPC-IRAS*  
END
```